

PLANNINGHANDBOOK

FIX'N SLIDE panel facade

SYSTEM WITH THERMAL SEPARATION FOR SECURE ATTACHMENT OF ADD-ON ELEMENTS TO THERMOPANEL BUILDING ENVELOPES



FOR HALL CONSTRUCTION

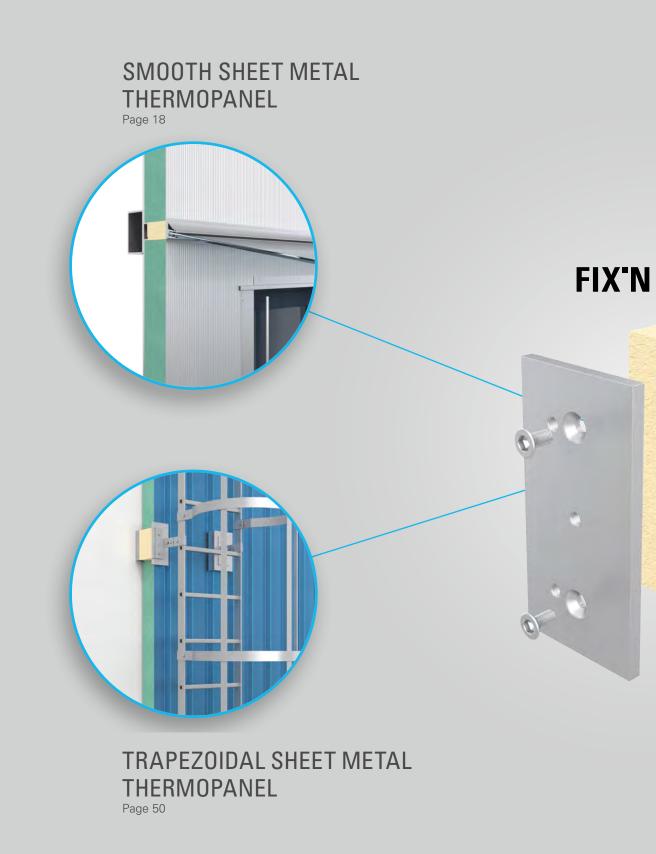
- Reduction of thermal bridges
- Secure attachment of add-on elements
- Thermal properties/ energy planning according to EnEV 2016
- Safe load introduction
- Variable attachment methods
- Modular and flexible
- Application-independent bridging of the insulation system
- Safety in case of fire
- Flexibly applicable for new constructions or retrofitting



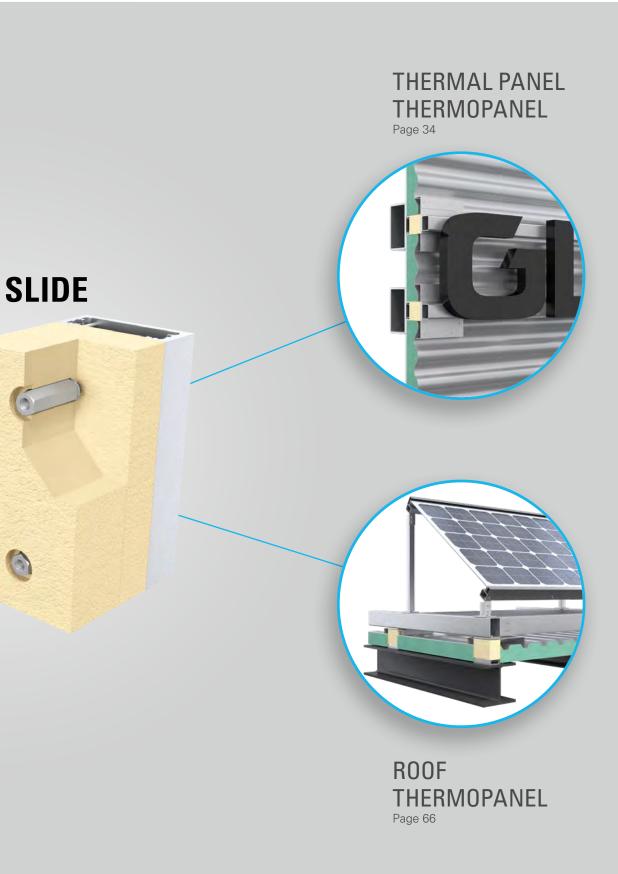














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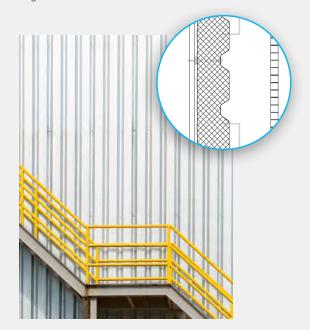
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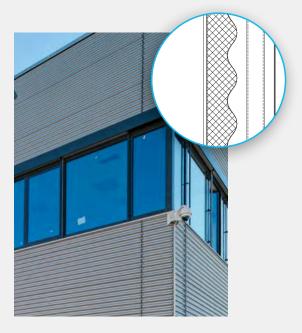
SMOOTH SHEET METAL

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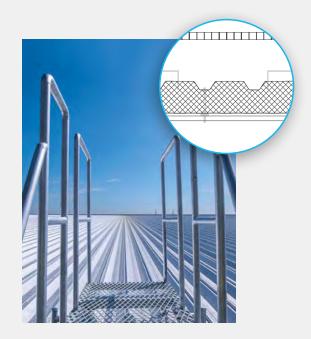
TRAPEZOIDAL SHEET METAL FACADE

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TRAPEZOIDAL SHEET METAL ROOF

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FIX'N SLIDE panel facade

COMPONENT ANCHORING WITH A SYSTEM THROUGH THE REDUCTION OF THERMAL BRIDGES

Flexible, easy to install and absolutely safe - the new FIX*N SLIDE revolutionises component assembly for thermopanel building envelopes. FIX*N SLIDE ensures the secure attachment of add-on elements and simultaneously reduces thermal bridges in new constructions and retrofitting.

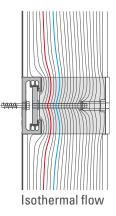
With just a few components and different insulation thicknesses, almost every thickness of a thermopanel wall canbe thermally and statically bridged. FIX*N SLIDE accommodates every on-site situation as a rail for linear assembly and as a system component for point-to-point mounting. Both designs can also be combined.



THE ADVANTAGES

FOR THERMOPANEL BUILDING ENVELOPES

- REDUCTION OF THERMAL BRIDGES
- SAFE ATTACHMENT OF ADD-ON ELEMENTS



Thermal properties/energy planning according to EnEV 2016

The existing isothermal calculations/thermal verifications prove that the use of FIX*N SLIDE reduces the thermal bridges to a minimum. The system is ideally suited to energy planning in new constructions or installation in existing structures.

Safe load application

The system allows for a broad spectrum of application through the introduction of traction, shearing and torques.

Variable attachment method

Through the variable arrangement of the attachment elements, the load application can be optimally tailored to the substructure and optimised and adapted to the local conditions.

Modular and flexible

The system is modularly built and as flexible as the application requires. The different insulation thicknesses allow for easy bridging of every insulation thickness up to 315 mm.

Application-independent bridging of the insulation system

The slide-in bearing elements with their tensile threaded rods can be flexibly adapted to the supporting profile by being shifted. This makes the mounting of the aluminium rail to the substructure independent of the attachment of the add-on elements.

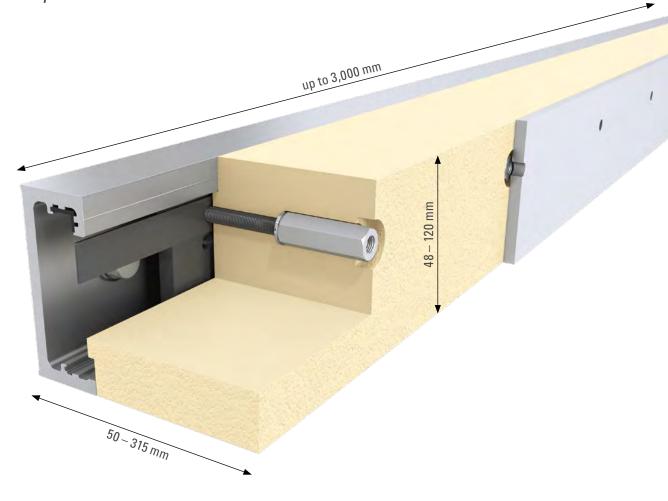
Safety in case of fire

In the event of failure, such as due to fire, constructive residual load-bearing capacity is guaranteed by the metallic supporting components.

Flexibly applicable – for new constructions or retrofitting

Advertising, canopies, awnings, photovoltaics and vertical ladders.



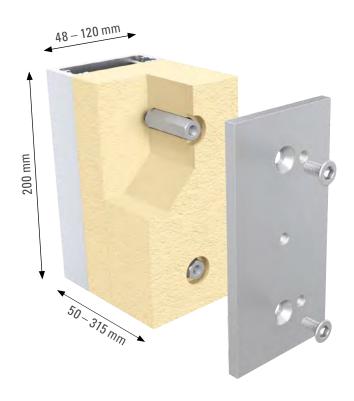


THE SYSTEM FOR LINEAR CONNECTION

The system is modularly built and as flexible as the application requires. The main components are application-independent aluminium rails for pre-assembly and connection to the substructure, slide-in plates made of stainless steel with tensile threaded rods and threaded sockets, pressure-resistant insulating elements and an optional aluminium connecting plate.

- Rails in fixed bearing lengths and individual lengths up to 3,000 mm
- 5 system widths from 48 to 120 mm
- The holes can be additionally variably bored for attachment of the rails
- Insulation thicknesses of 50 to 315 mm
- Slide-in plates with tensile threaded rods can be adapted to the attachment points of the add-on elements by being shifted
- Optional aluminium flush plaster/connecting plate (8 mm thickness) with self-adhesive EPDM tape for outdoor use
- Pre-drilled insulating element for the mounting of threaded rods and threaded sockets,
 additional holes can be variably drilled





SYSTEM COMPONENT WITH ADAPTOR PLATES FOR POINT-TO-POINT CONNECTION

Strictly defined complete system. The main components are the C profile for pre-assembly and connection to the substructure, two slide-in plates made of stainless steel with tensile threaded rods and threaded sockets, pressure-resistant insulating elements and optional stainless steel adaptor plates.

- Length 200 mm
- 5 system widths from 48 to 120 mm
- Strictly defined holes for attachment of the profile
- Insulation thicknesses of 50 to 315 mm
- Pre-drilled insulating elements for the mounting of the threaded rods and threaded sockets
- Optional stainless steel adaptor plates
- The attachment can also be used with or without on-site adaptor plates

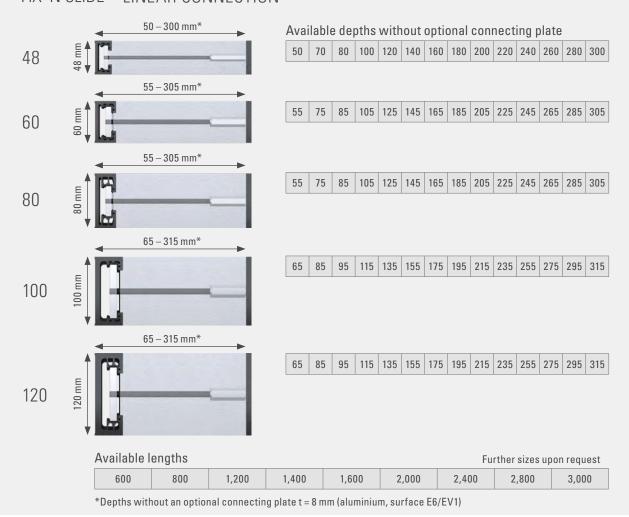


THE SYSTEM

FOR LINEAR CONNECTION



FIX N SLIDE - LINEAR CONNECTION



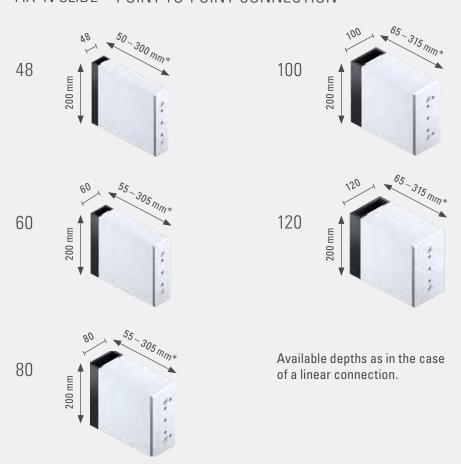


FOR POINT-TO-POINT CONNECTION

The system component can also be used with or without on-site adaptor plates for flexible mounting of attachments.



FIX N SLIDE - POINT-TO-POINT CONNECTION



^{*}Depths without an optional adaptor plate in stainless steel: 48, 60, 80 = 8 mm/100, 120 = 10 mm

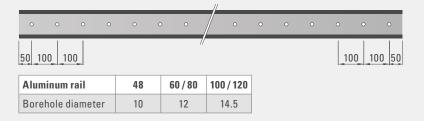


BOREHOLE SPACINGS



LINEAR CONNECTION

ALUMINIUM RAIL BOREHOLE PATTERN



BOREHOLE PATTERN FOR INSULATING BLOCK AND CONNECTING PLATES (ALU)

All system widths Centred boreholes

0	O	0	./.	0	•	0
100	200	200	//	200	200	100

System widths 100

Off-centre boreholes

Ideal for the GLASSLINE all-glass canopy system CANOPY CLOUD (profile type 1)

0	0	0	./.	0	0	•
100	200	200	_//	200	200	100

System widths 120

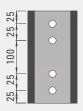
Off-centre boreholes

Ideal for the GLASSLINE all-glass canopy system CANOPY CLOUD (profile type 3)

0	0	0	•/-	•	•	•
100 200	200		//	200	200	100

POINT-TO-POINT CONNECTION

ALUMINIUM RAIL BOREHOLE PATTERN



Aluminum rail	48	60/80	100 / 120
Borehole diameter	10	12	14.5

BOREHOLE PATTERN FOR INSULATING BLOCK WITH ADAPTOR PLATE





STAINLESS STEEL ADAPTOR PLATES

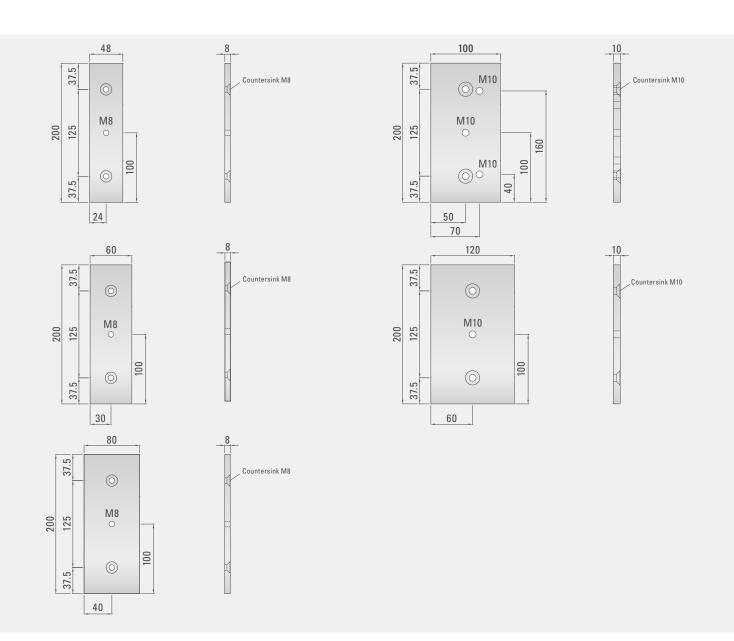








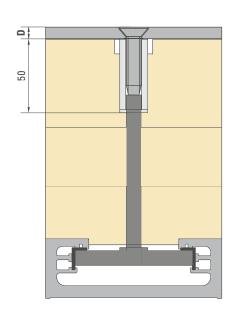


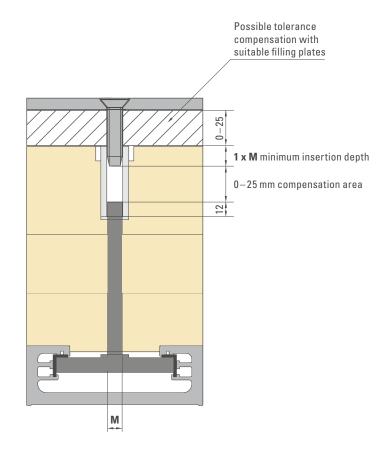




LEVEL COMPENSATION

WITH ON-SITE RELINING





Size	М	D
48	8	8
60	8	8
80	8	8
100	10	10
120	10	10



VARIO SYSTEM MODULE

INFINITELY ADJUSTABLE FOR INTERIOR CONSTRUCTION



 $0-30 \; \text{mm}$ compensation area

The infinitely adjustable FIX*N SLIDE VARIO system module allows for the precise compensation of height differences in the on-site foundation of up to 30 mm in the mounting of wall elements, support posts and other components.



Screw 6 pressure pins into the base plate



Place the compensating plate with 2 screw connections on to the base plate



Screw both screw connections to the desired height



Move the compensating plate upwards against the screw connection using the pressure elements



Insertion of the 2 locking pins







INDUSTRIAL HALL WITH SMOOTH SHEET METAL THERMOPANEL AND CANOPY CLOUD

APPLICATION EXAMPLES

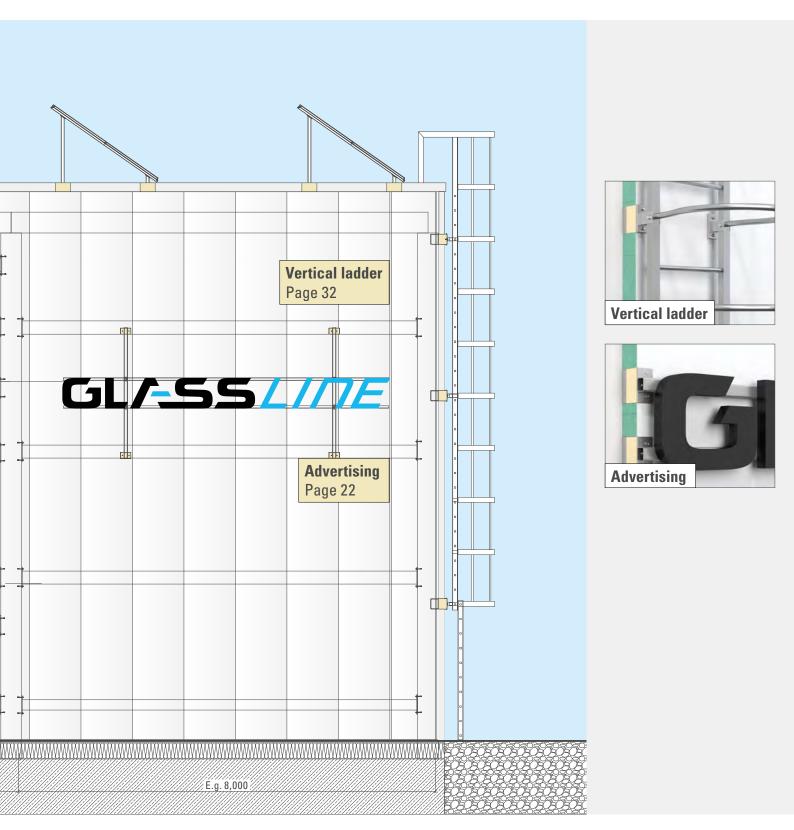


View of an industrial hall

with smooth sheet metal thermopanel





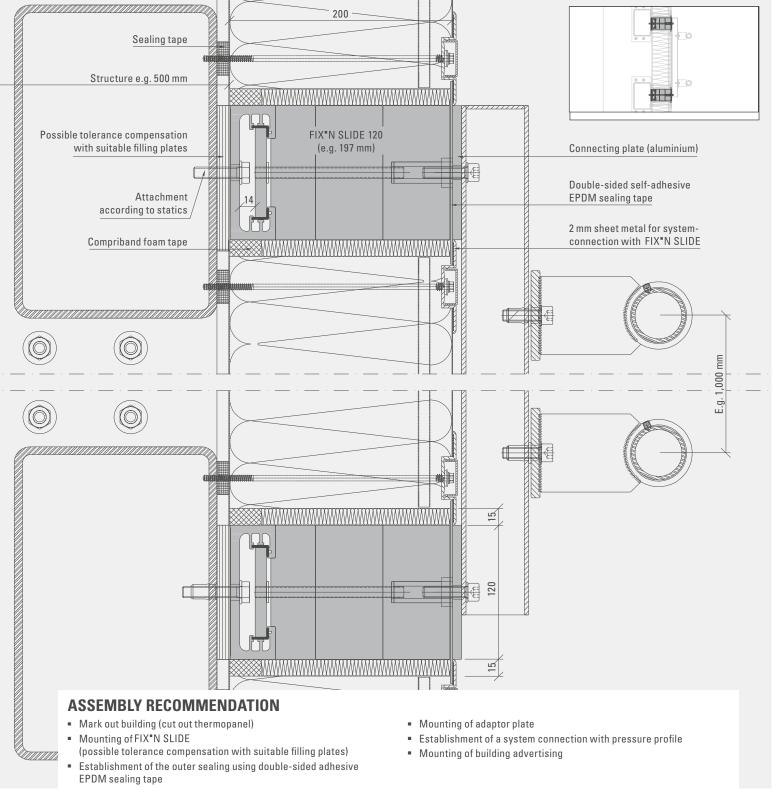




Advertising on an industrial hall

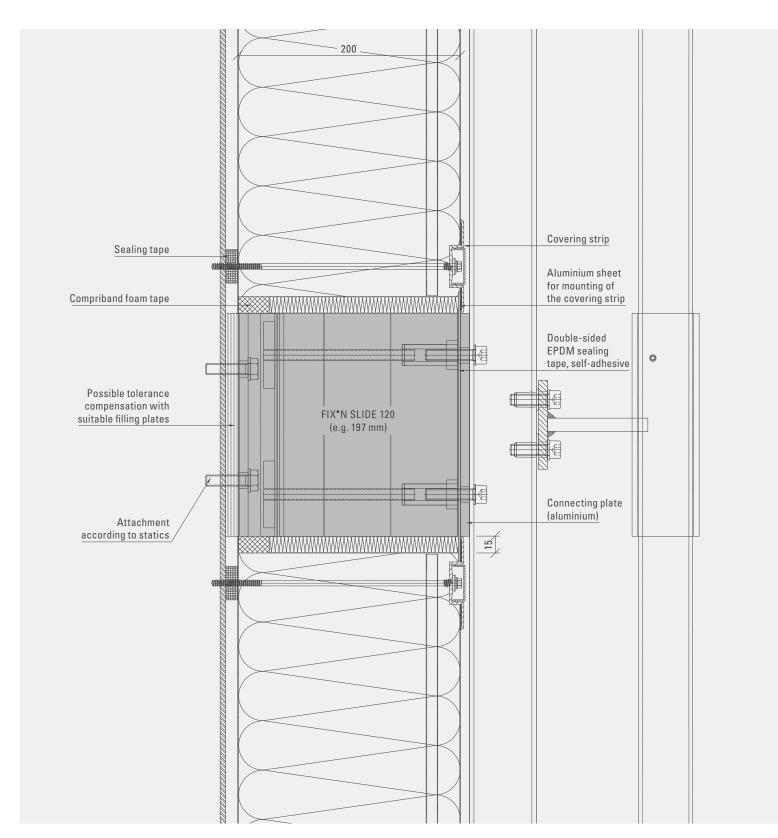
Smooth sheet metal sandwich panel facade

Vertical section





Horizontal section

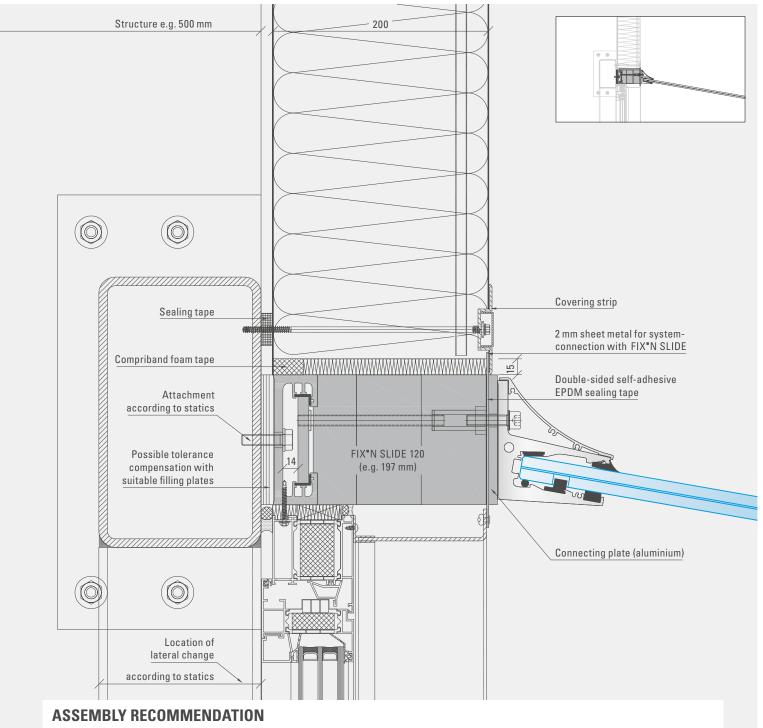




Glass canopy CANOPY CLOUD

Smooth sheet metal thermowall with door element

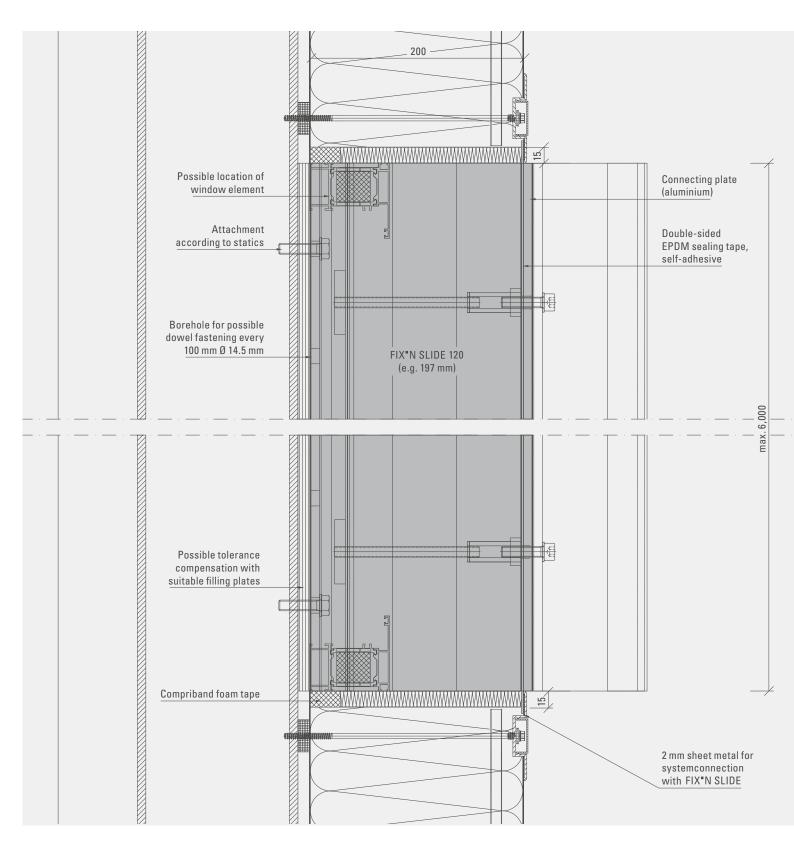
Vertical section



- Mark out building (determine outer edge insulation)
- Mounting of FIX*N SLIDE (possible tolerance compensation with suitable filling plates)
- Establishment of the outer sealing using double-sided adhesive EPDM sealing tape
- Connecting plate fixation
- Building of the thermopanel façade
- Installation of the door including panelling
- Mounting of the canopy



Horizontal section

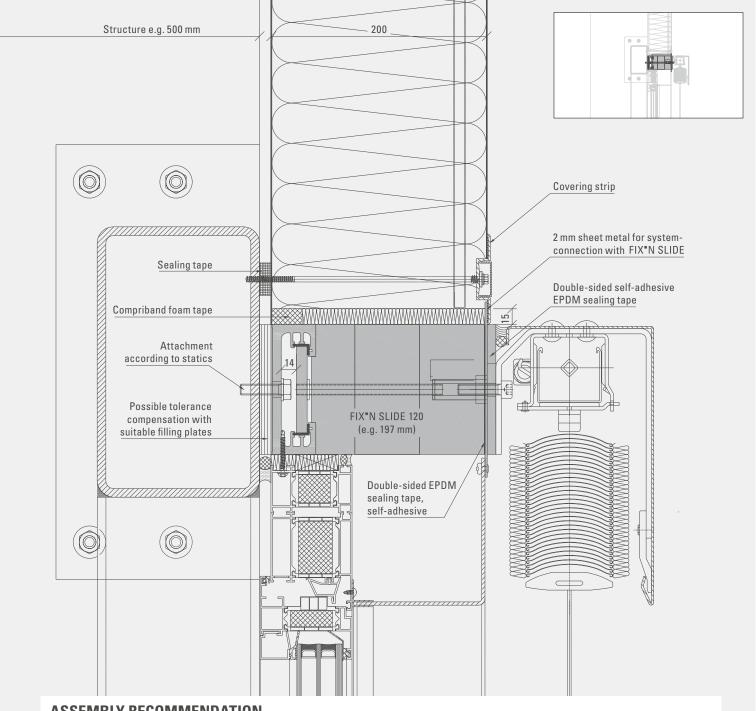




Upper connection of the **Venetian blind** with cable guide

Window element in the smooth sheet metal thermopanel

Vertical section

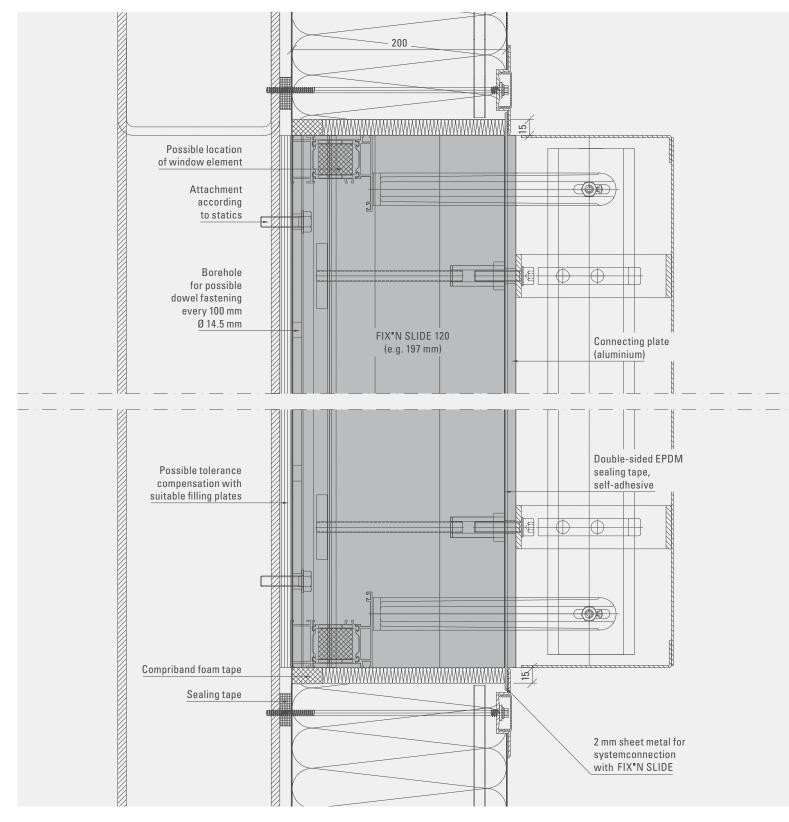


ASSEMBLY RECOMMENDATION

- Mark out building (determine outer edge insulation)
- Mounting of FIX*N SLIDE (possible tolerance compensation with suitable filling plates)
- Establishment of the outer sealing using double-sided adhesive EPDM sealing tape
- Connecting plate fixation
- Building of the thermopanel façade
- Installation of window element including panelling
- Mounting of sunscreen



Horizontal section

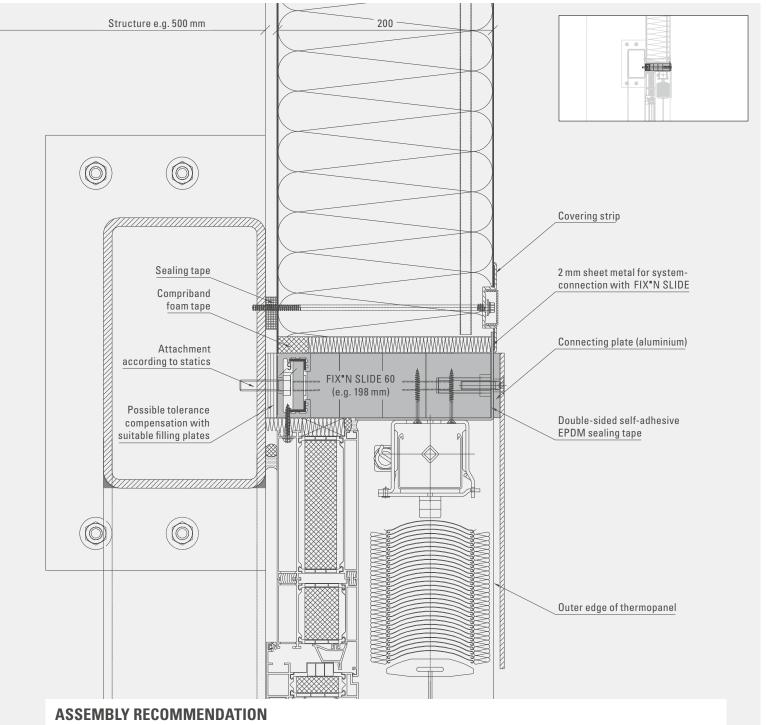




Venetian blind with cable guide

Smooth sheet metal thermopanel in the soffit

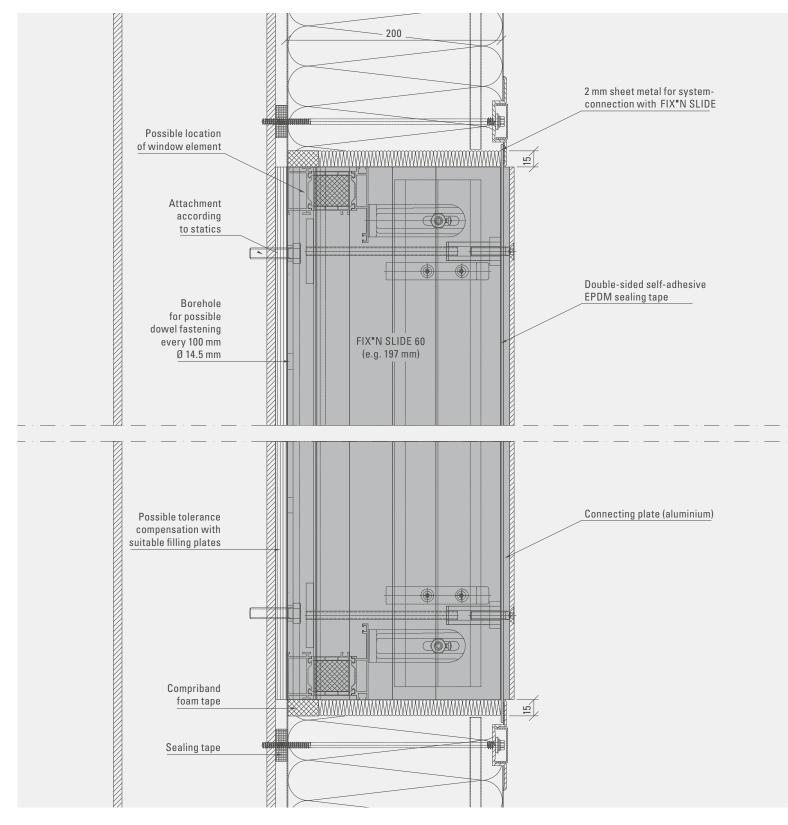
Vertical section



- Mark out building (determine outer edge insulation)
- Mounting of FIX*N SLIDE (possible tolerance compensation with suitable filling plates)
- Establishment of the outer sealing using double-sided adhesive EPDM sealing tape
- Connecting plate fixation
- Building of the thermopanel façade
- Installation of window element including panelling
- Mounting of sunscreen



Horizontal section

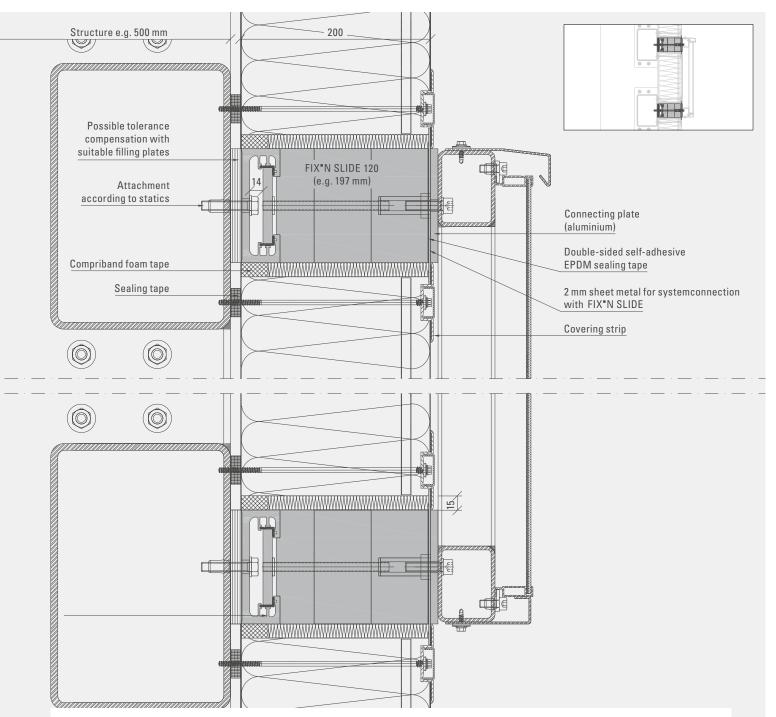




Photovoltaic modules on the substructure

Smooth sheet metal thermopanel

Vertical section

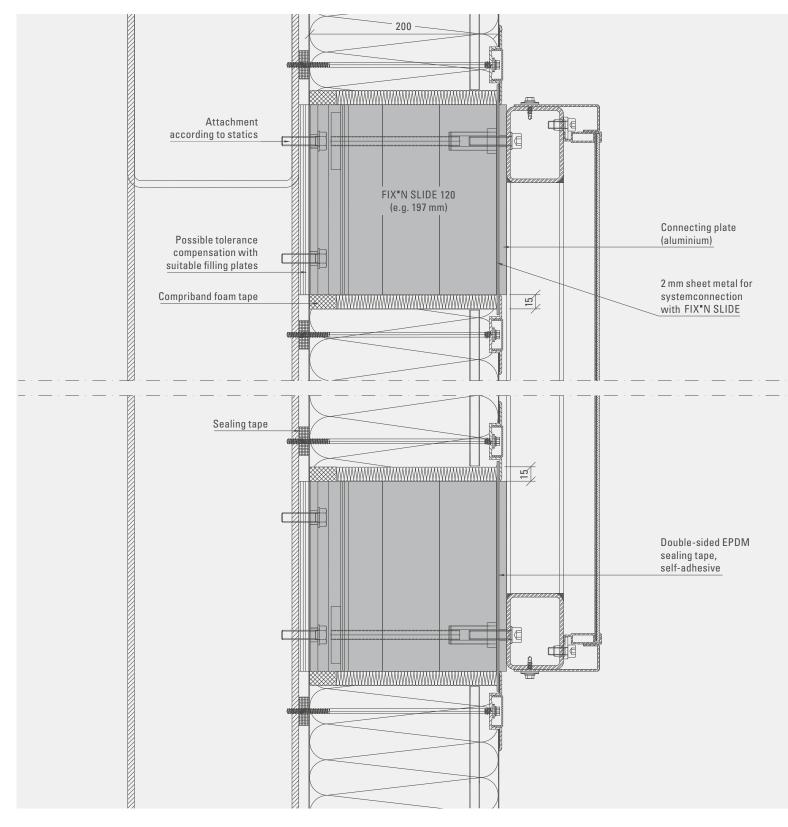


ASSEMBLY RECOMMENDATION

- Mark out building (determine outer edge insulation)
- Mounting of FIX*N SLIDE (possible tolerance compensation with suitable filling plates)
- Establishment of the outer sealing using double-sided adhesive EPDM sealing tape
- Connecting plate fixation
- Building of the thermopanel façade
- Installation of window element including panelling
- Installation of photovoltaic system



Horizontal section

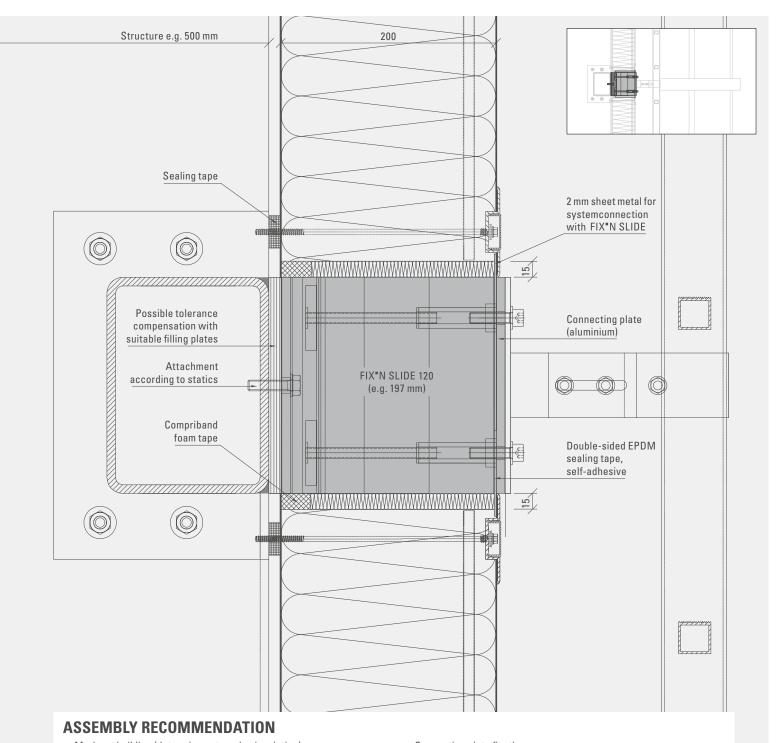




Fixed ladder DIN 18799-1

Smooth sheet metal thermopanel

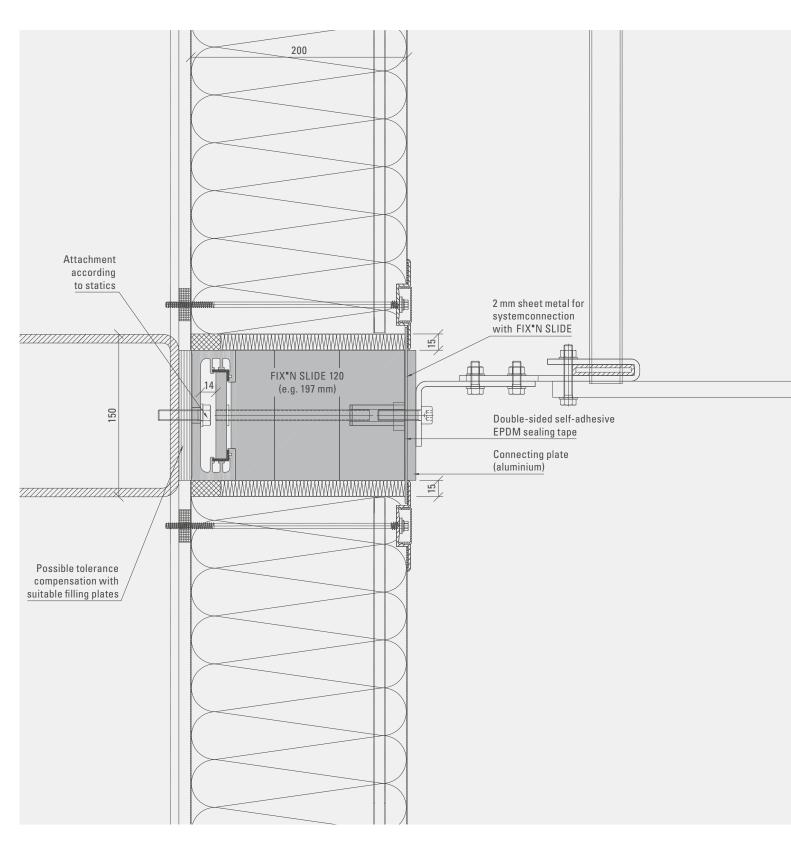
Vertical section



- Mark out building (determine outer edge insulation)
- Mounting of FIX*N SLIDE (possible tolerance compensation with suitable filling plates)
- Establishment of the outer sealing using double-sided adhesive EPDM sealing tape
- Connecting plate fixation
- Building of the thermopanel façade
- Installation of the vertical ladder



Horizontal section









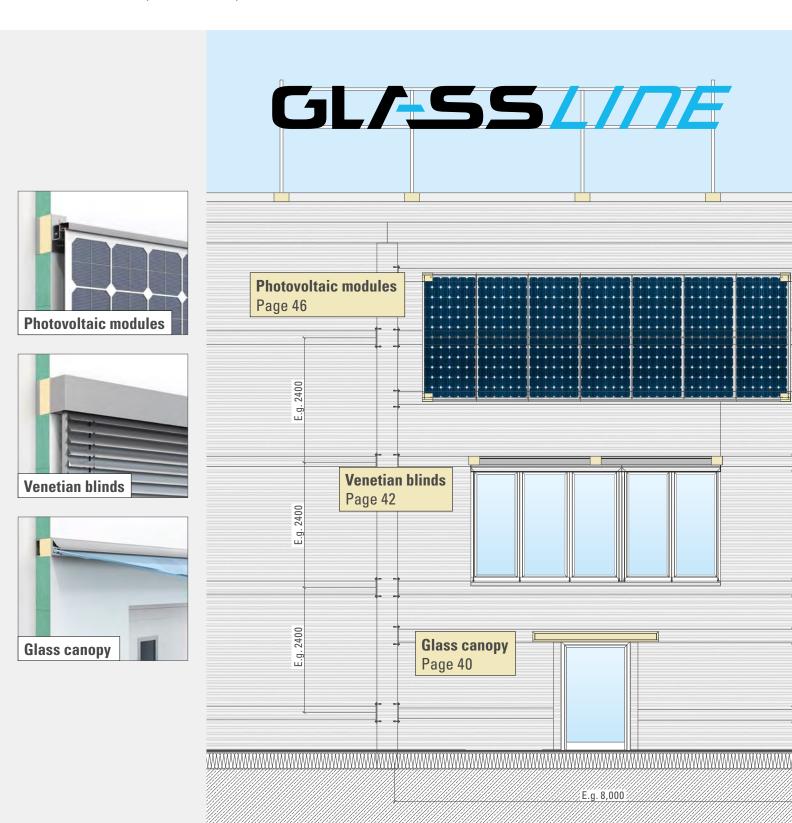
INDUSTRIAL HALL WITH THERMAL PANEL THERMOPANEL AND ADVERTISING MEDIUM

APPLICATION EXAMPLES

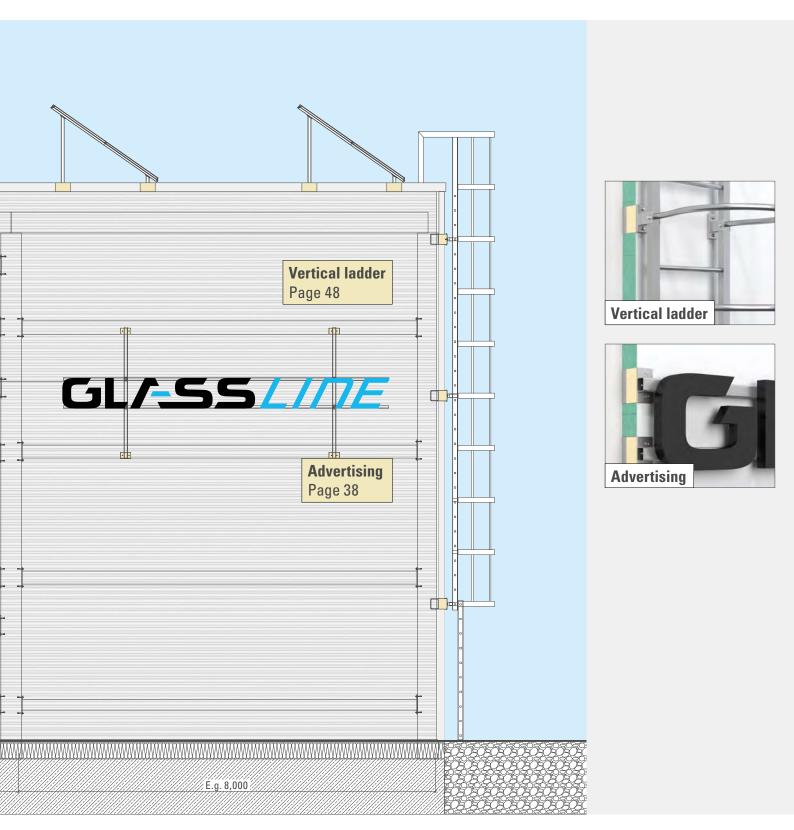


View of an industrial hall

with thermal panel thermopanel





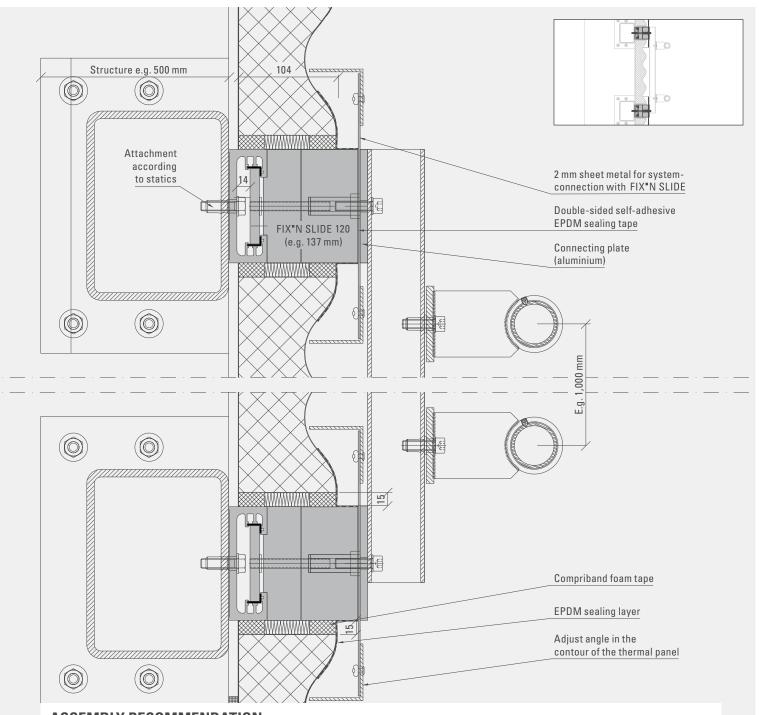




Advertising on an industrial hall

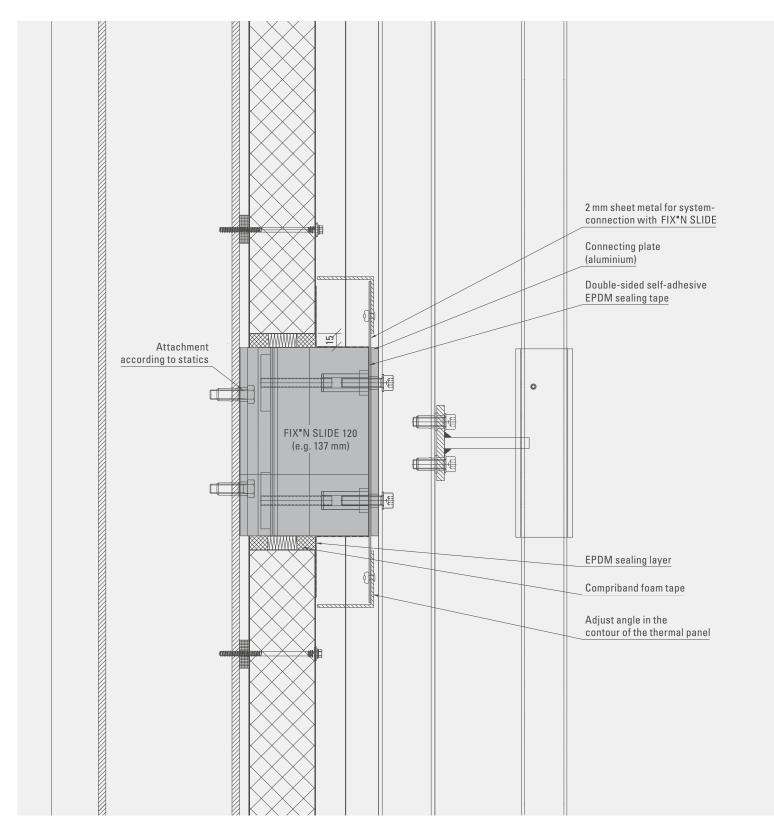
Thermal panel thermopanel

Vertical section



- Mark out building (determine outer edge insulation)
- Mounting of FIX*N SLIDE (possible tolerance compensation with suitable filling plates)
- Establishment of the outer sealing using double-sided adhesive EPDM sealing tape
- Connecting plate fixation
- Building of the thermopanel façade
- Mounting of the advertising medium



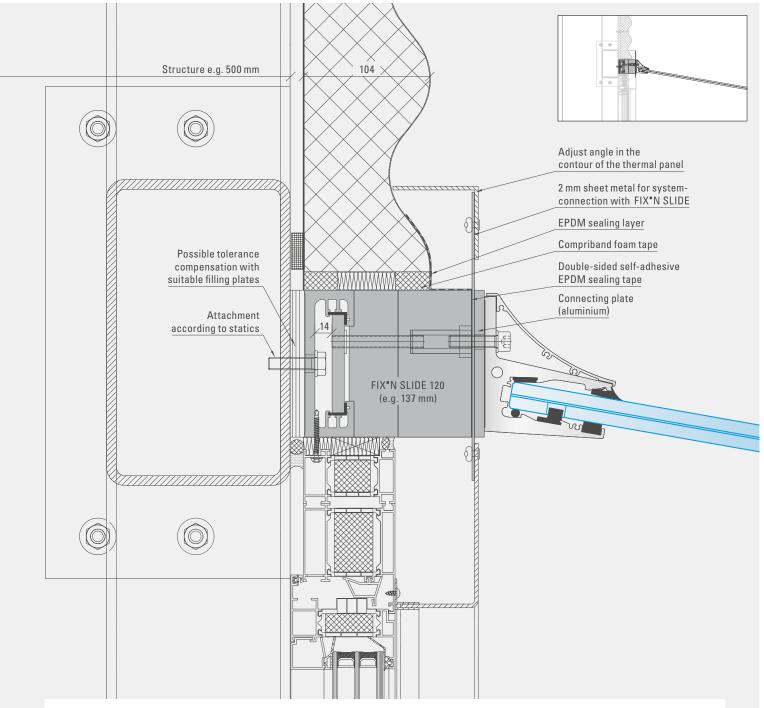




Glass canopy CANOPY CLOUD

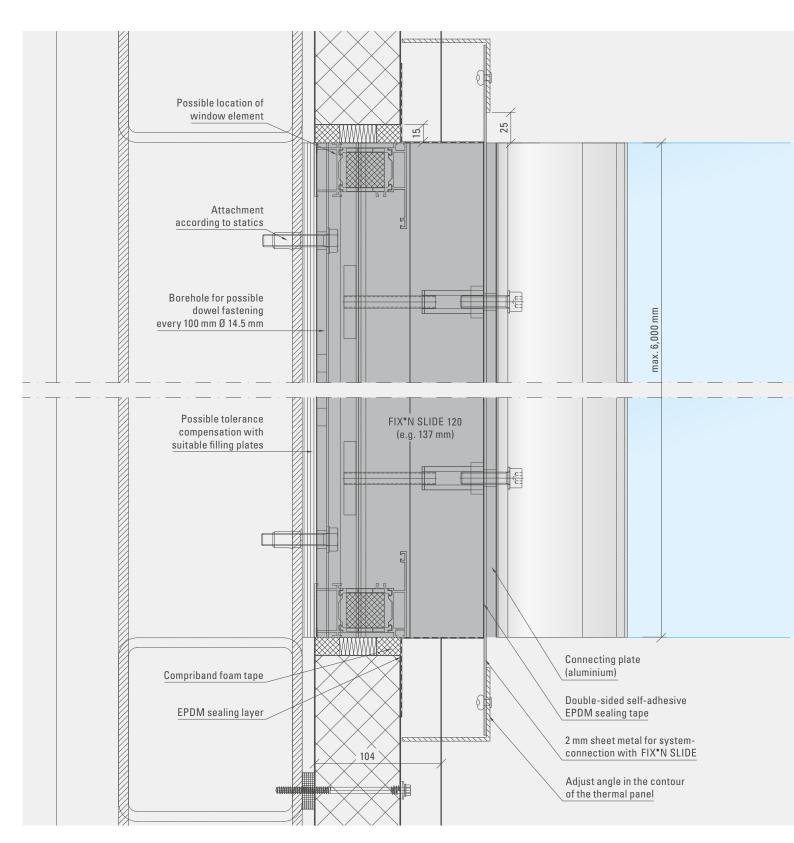
Thermal panel thermopanel with door element

Vertical section



- Mark out building (determine outer edge insulation)
- Mounting of FIX*N SLIDE (possible tolerance compensation with suitable filling plates)
- Establishment of the outer sealing using double-sided adhesive EPDM sealing tape
- Connecting plate fixation
- Building of the thermopanel façade
- Mounting of the canopy



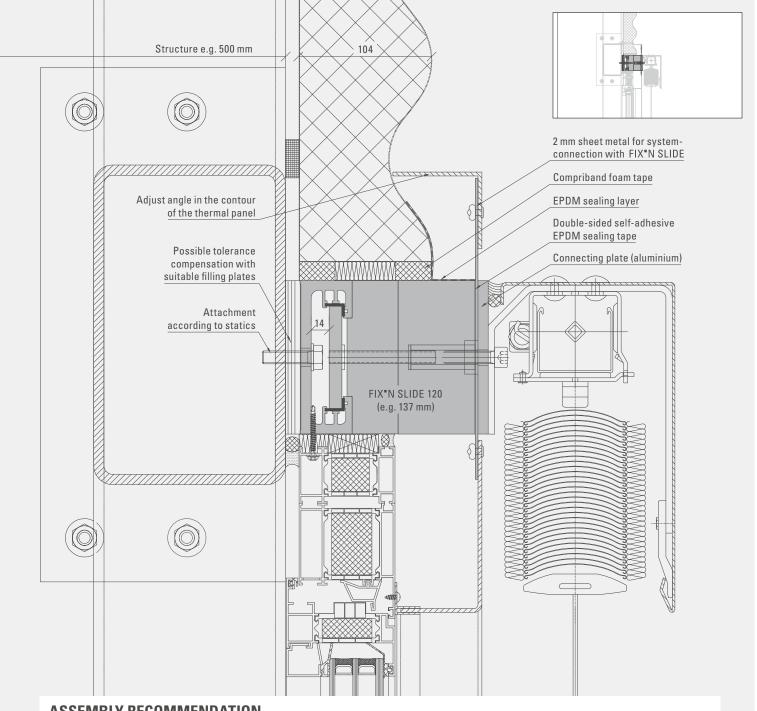




Upper connection of the **Venetian blind** with cable guide

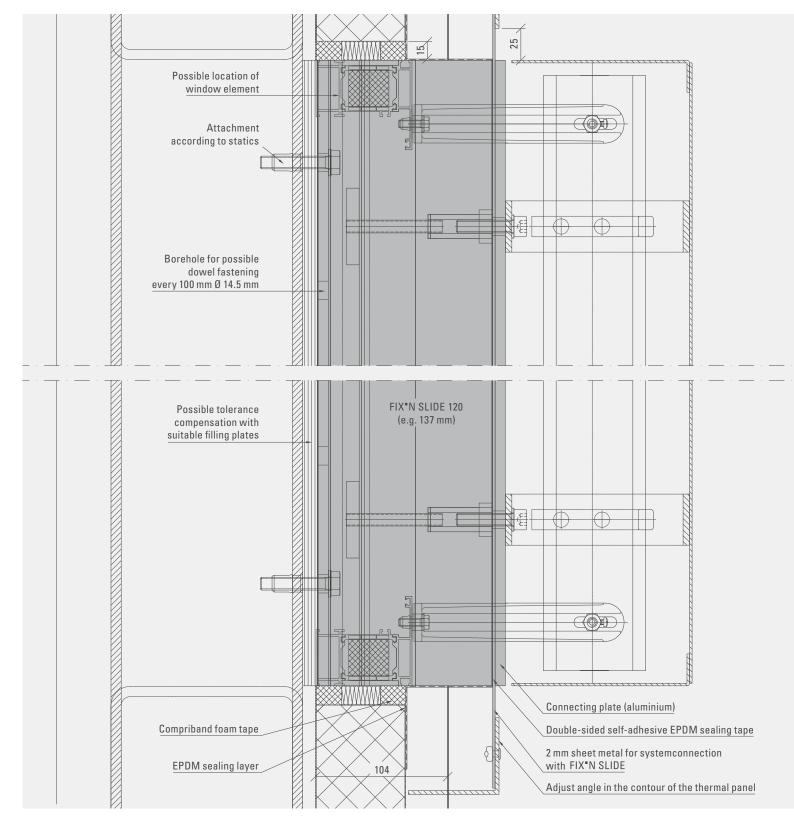
Window element in thermal panel thermopanel

Vertical section



- Mark out building (determine outer edge insulation)
- Mounting of thermopanel FIX*N SLIDE (possible tolerance compensation with suitable filling plates)
- Establishment of the outer sealing using double-sided adhesive EPDM sealing tape
- Connecting plate fixation
- Building of the thermopanel façade
- Mounting of sunscreen



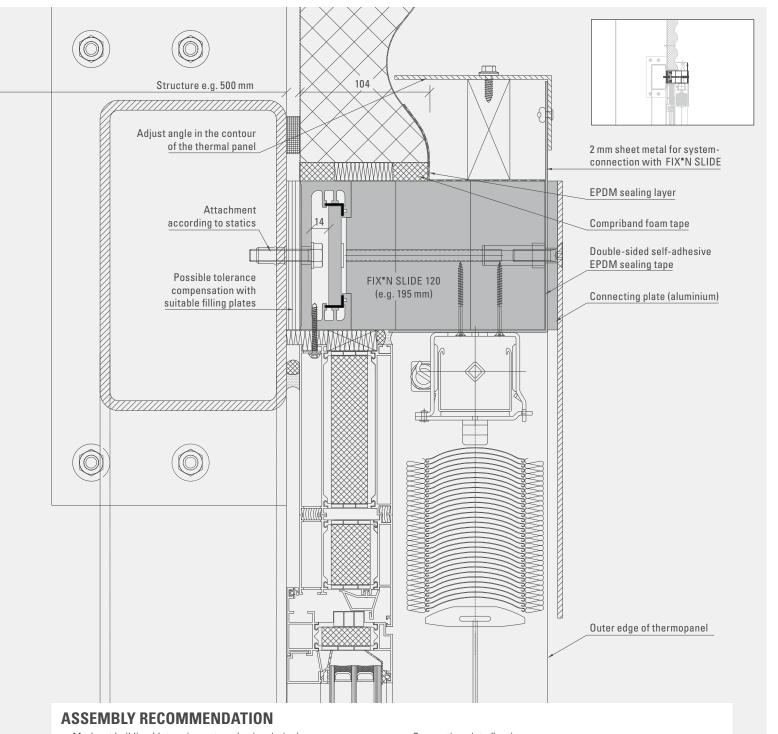




Venetian blind with cable guide

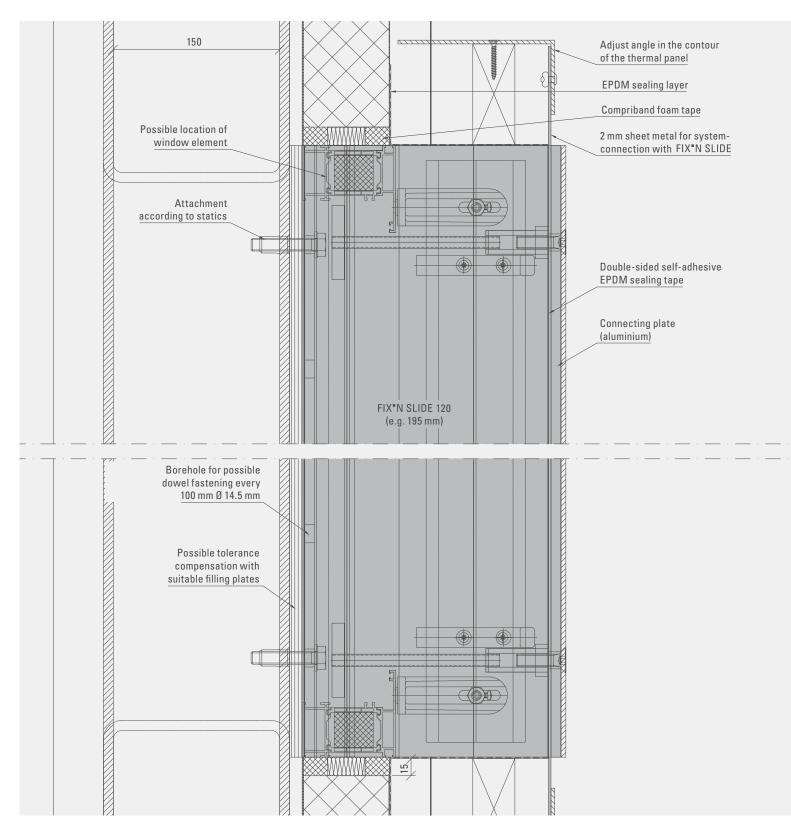
Smooth sheet metal thermopanel in the soffit

Vertical section



- Mark out building (determine outer edge insulation)
- Mounting of thermopanel FIX*N SLIDE (possible tolerance compensation with suitable filling plates)
- Establishment of the outer sealing using double-sided adhesive EPDM sealing tape
- Connecting plate fixation
- Building of the thermopanel façade
- Mounting of sunscreen



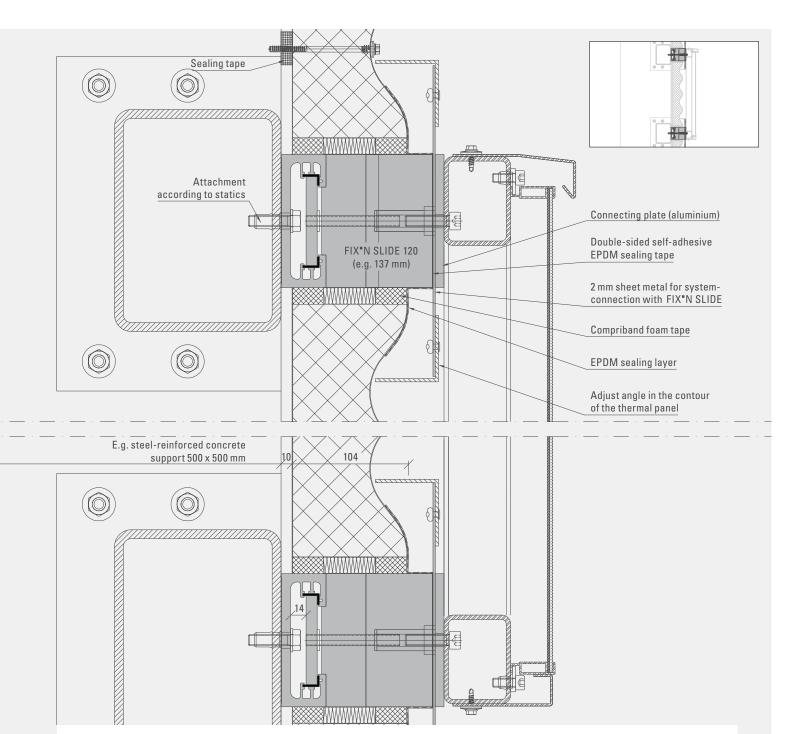




Photovoltaic modules on the substructure

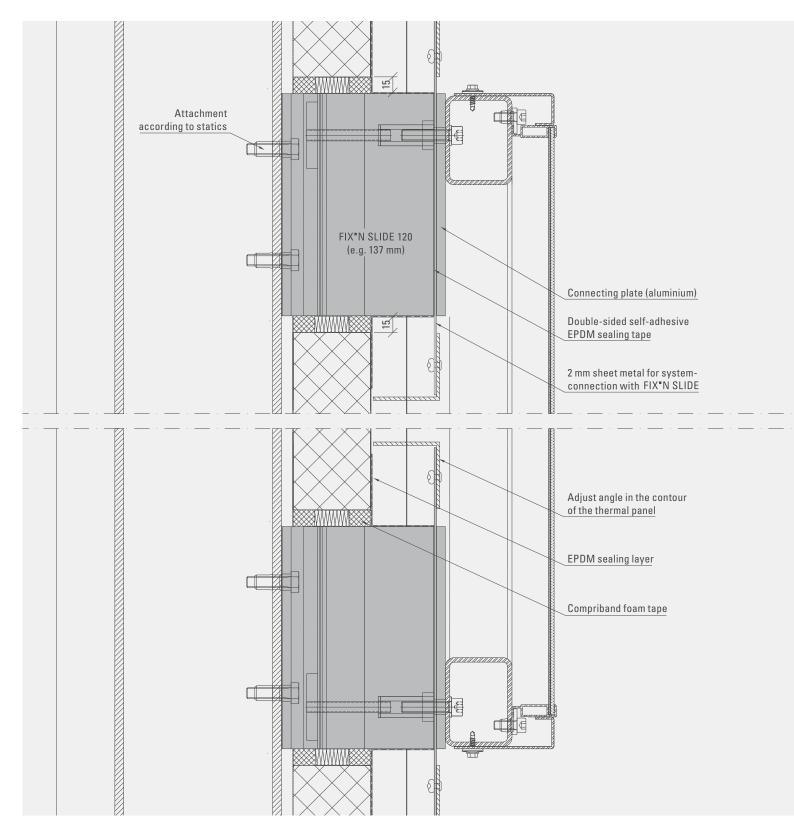
Thermal panel thermopanel

Vertical section



- Mark out building (determine outer edge insulation)
- Mounting of thermopanel FIX*N SLIDE (possible tolerance compensation with suitable filling plates)
- Establishment of the outer sealing using double-sided adhesive EPDM sealing tape
- Connecting plate fixation
- Building of the thermopanel façade
- Mounting of photovoltaic modules



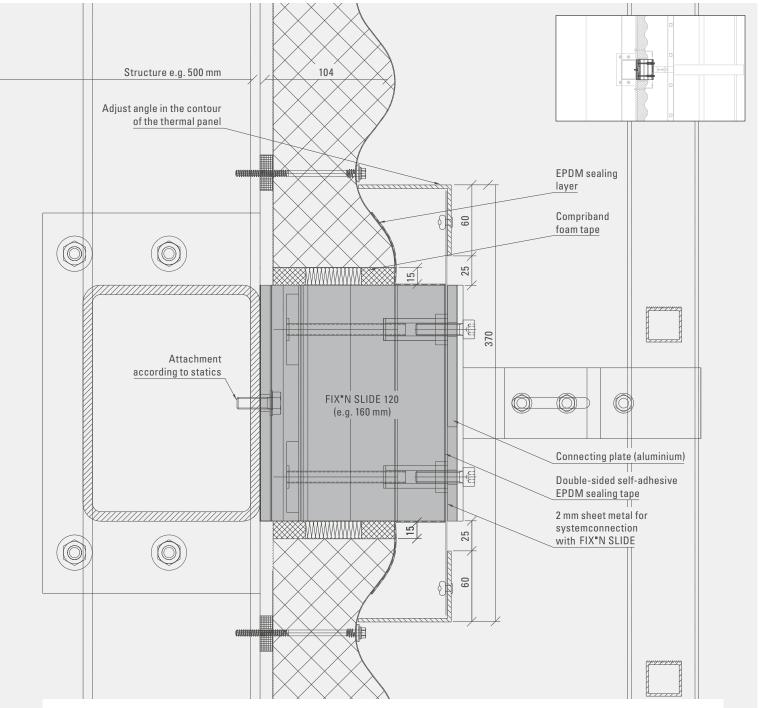




Fixed ladder DIN 18799-1

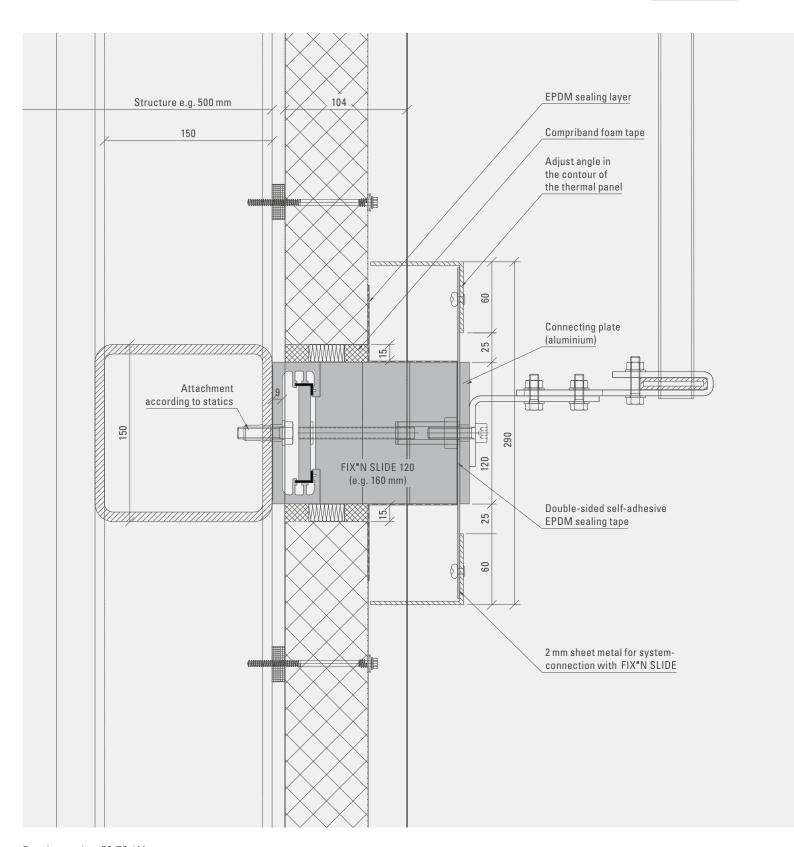
Thermal panel thermopanel

Vertical section

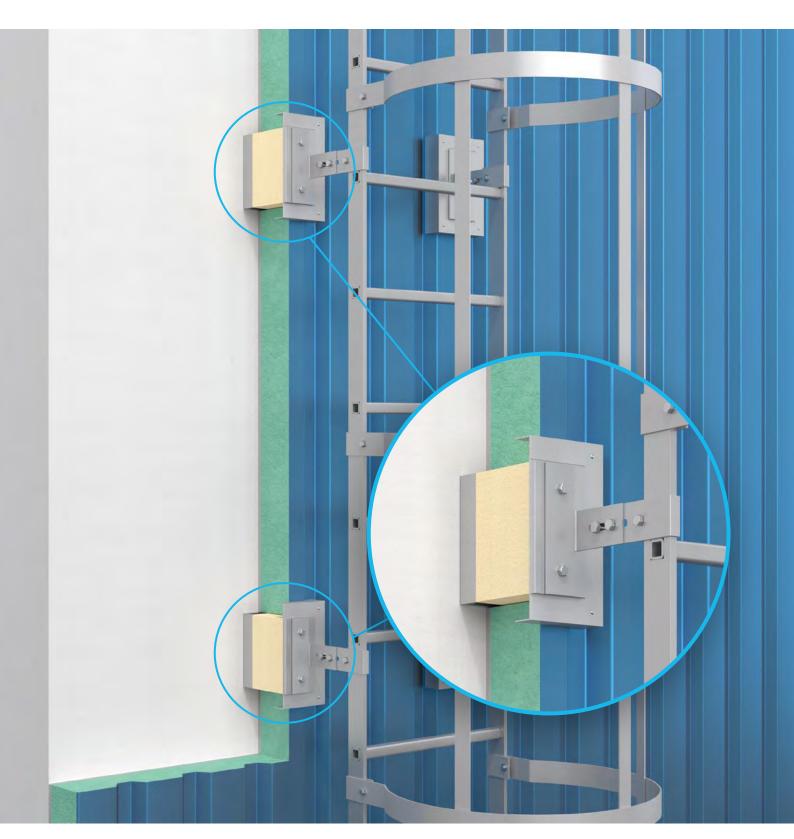


- Mark out building (determine outer edge insulation)
- Mounting of thermopanel FIX*N SLIDE (possible tolerance compensation with suitable filling plates)
- Establishment of the outer sealing using double-sided adhesive EPDM sealing tape
- Connecting plate fixation
- Building of the thermopanel façade
- Installation of vertical ladder











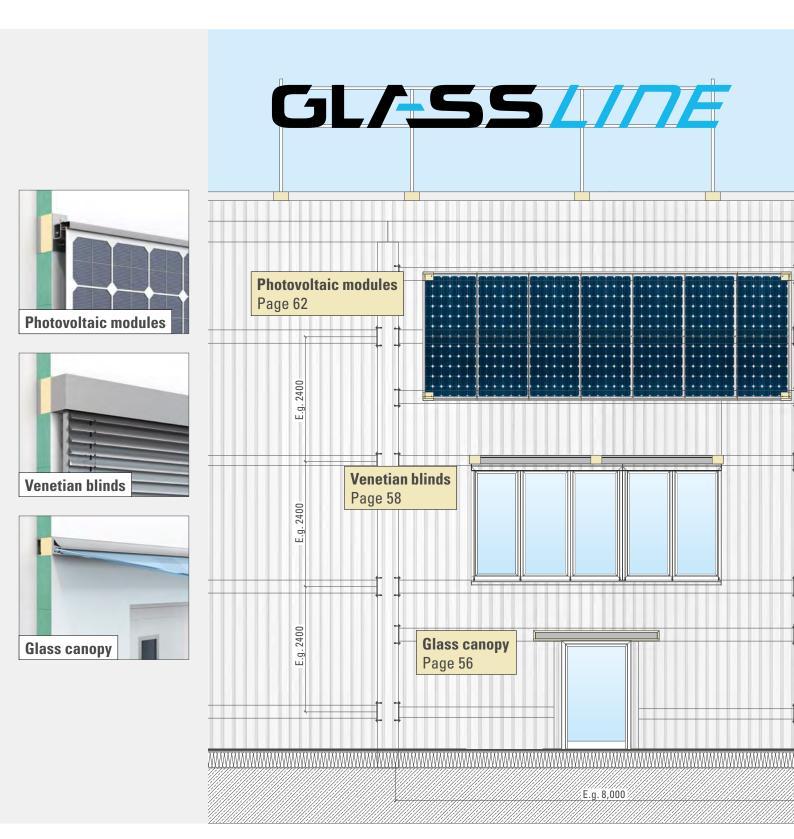
INDUSTRIAL HALL WITH TRAPEZOIDAL SHEET METAL THERMOPANEL AND VERTICAL LADDER

APPLICATION EXAMPLES

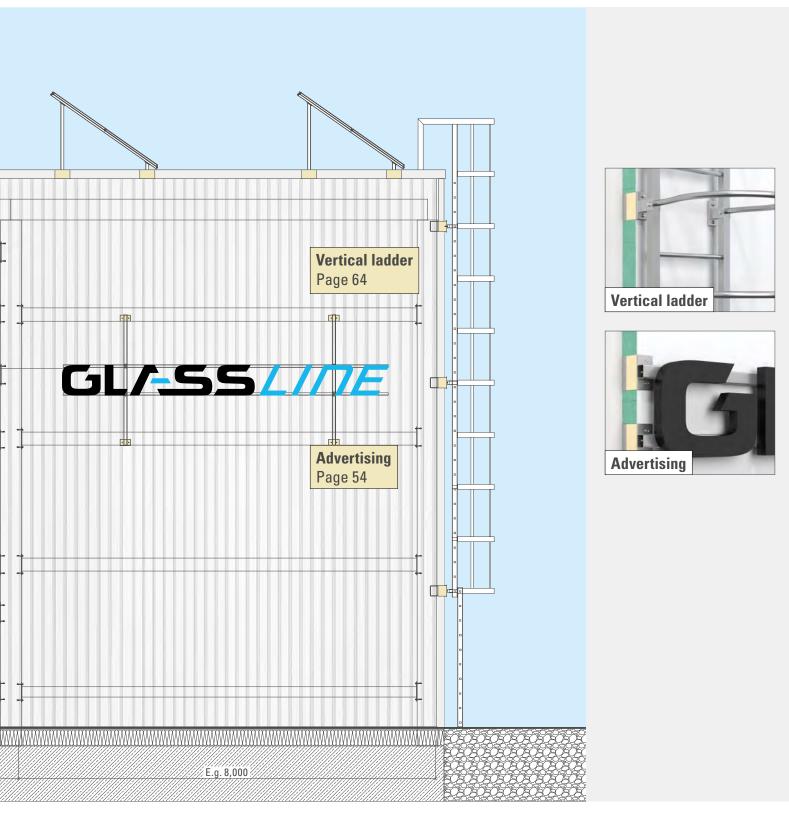


View of an industrial hall

with trapezoidal sheet metal thermopanel





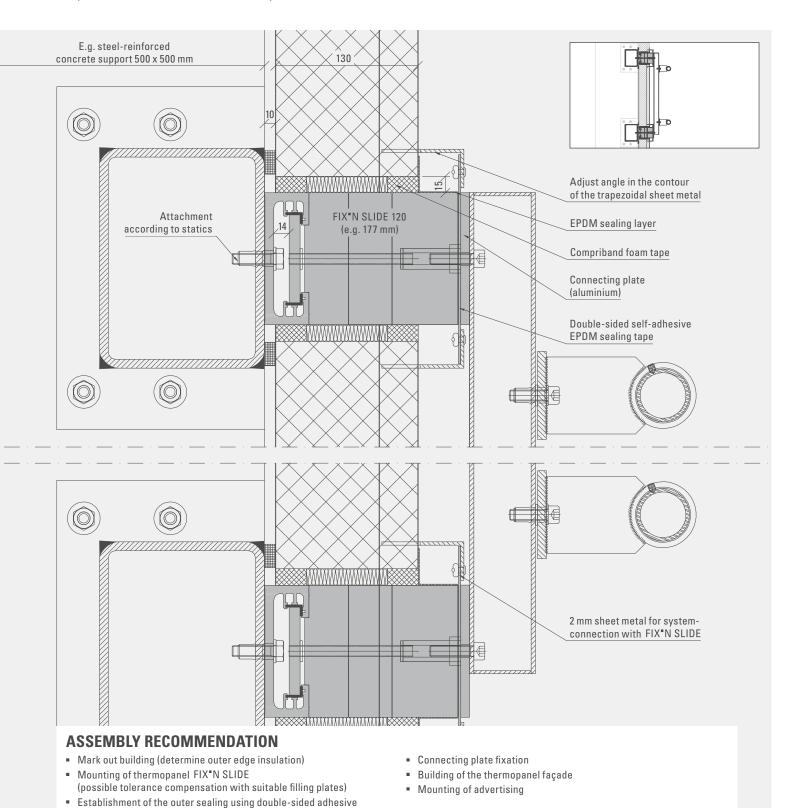




Advertising on sandwich panel façade

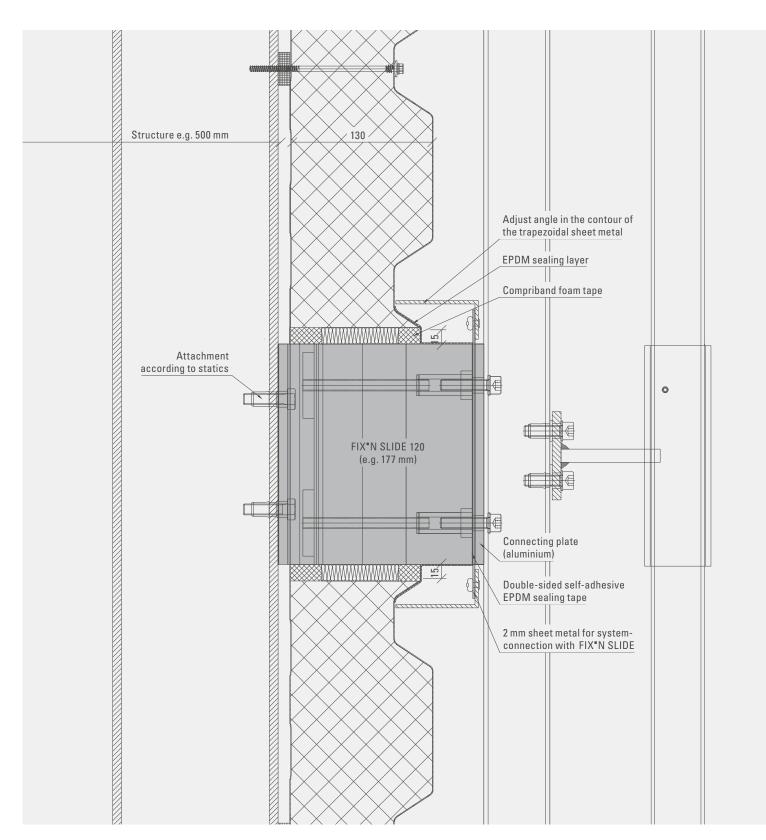
Trapezoidal sheet metal thermopanel

Vertical section



EPDM sealing tape



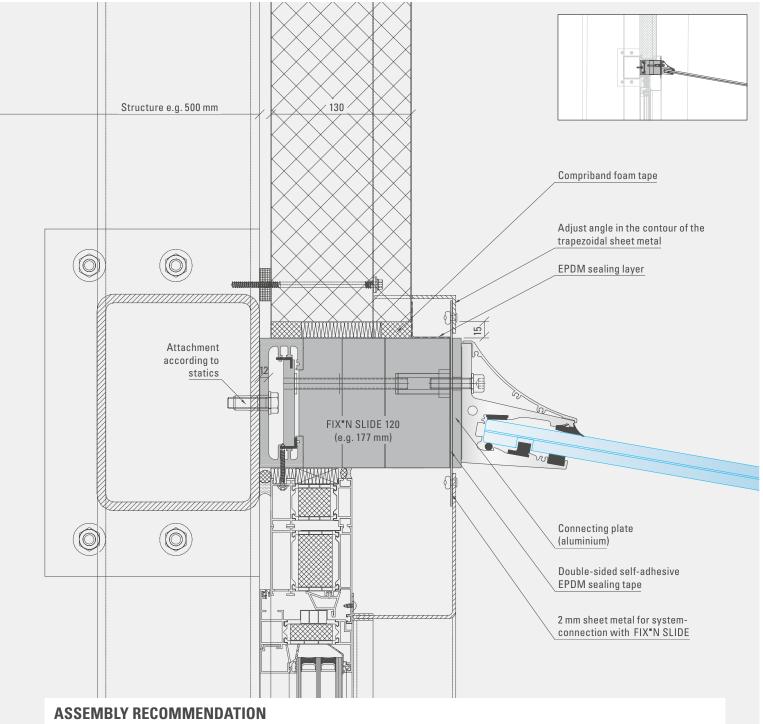




Glass canopy CANOPY CLOUD

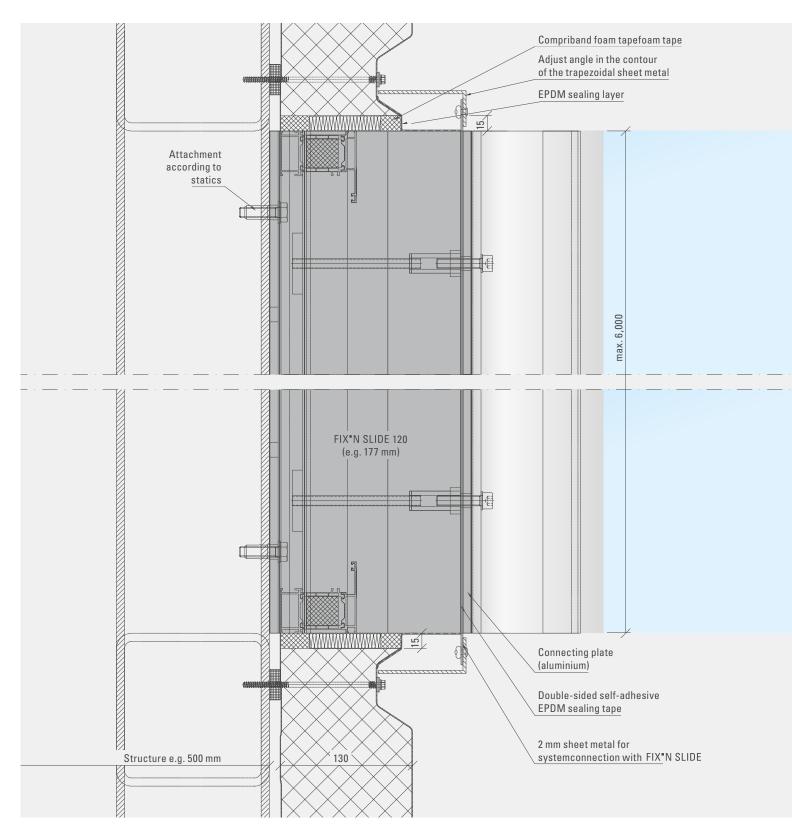
Trapezoidal sheet metal thermopanel with door element

Vertical section



- Mark out building (determine outer edge insulation)
- Mounting of thermopanel FIX*N SLIDE (possible tolerance compensation with suitable filling plates)
- Establishment of the outer sealing using double-sided adhesive EPDM sealing tape
- Connecting plate fixation
- Building of the thermopanel façade
- Mounting of the canopy



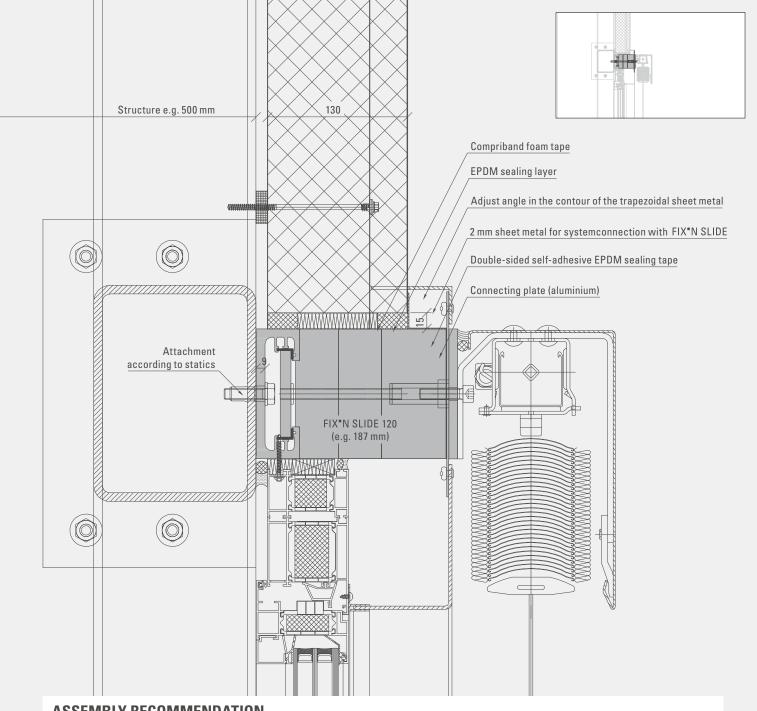




Upper connection of the **Venetian blind** with cable guide

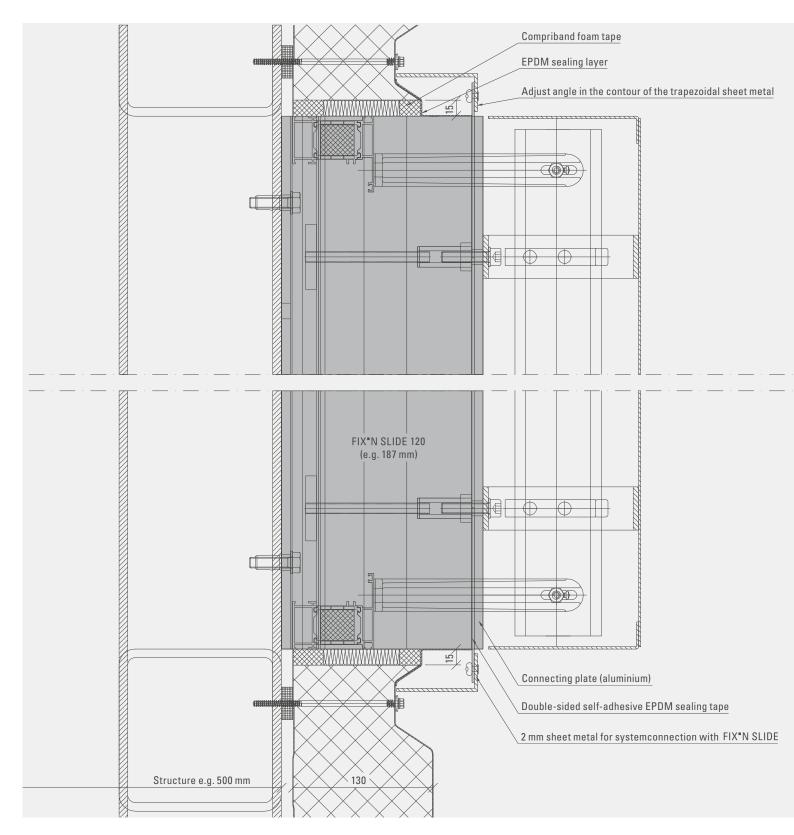
Window element in trapezoidal sheet metal thermopanel

Vertical section



- Mark out building (determine outer edge insulation)
- Mounting of thermopanel FIX*N SLIDE (possible tolerance compensation with suitable filling plates)
- Establishment of the outer sealing using double-sided adhesive EPDM sealing tape
- Connecting plate fixation
- Building of the thermopanel façade
- Mounting of sunscreen



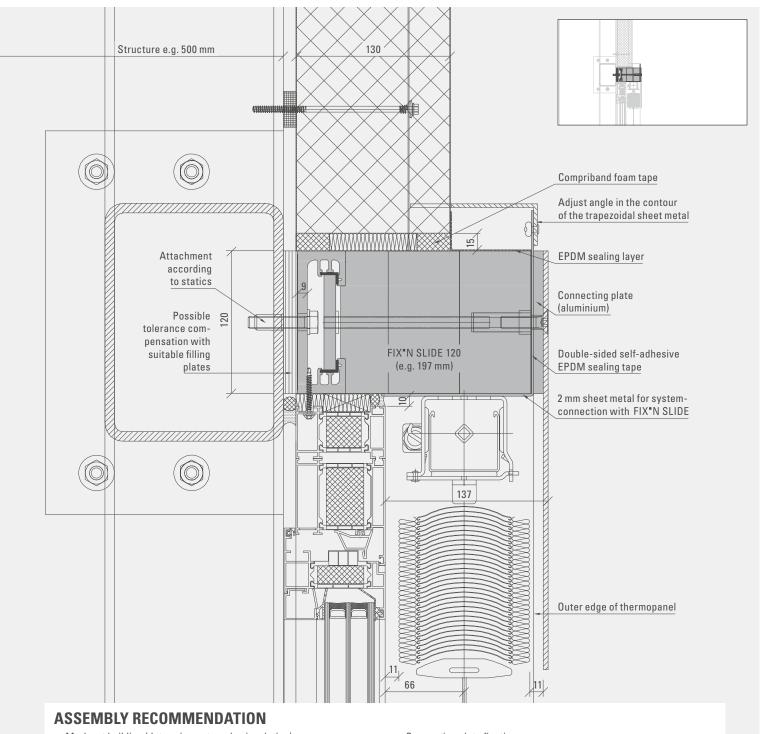




Venetian blind with cable guide

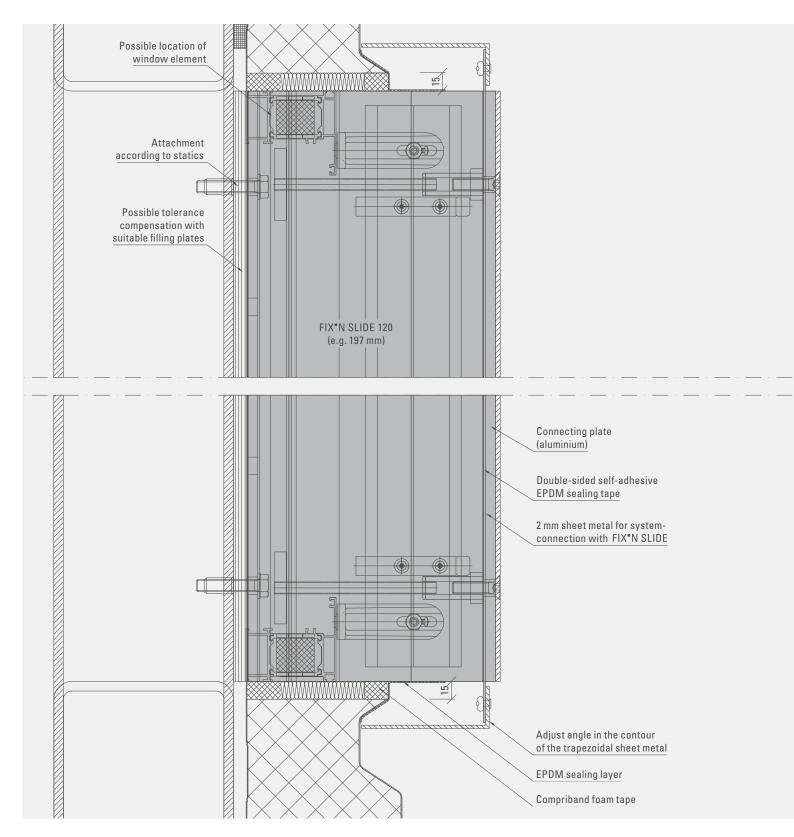
Smooth sheet metal thermopanel in the soffit

Vertical section



- Mark out building (determine outer edge insulation)
- Mounting of thermopanel FIX*N SLIDE (possible tolerance compensation with suitable filling plates)
- Establishment of the outer sealing using double-sided adhesive EPDM sealing tape
- Connecting plate fixation
- Building of the thermopanel façade
- Mounting of sunscreen



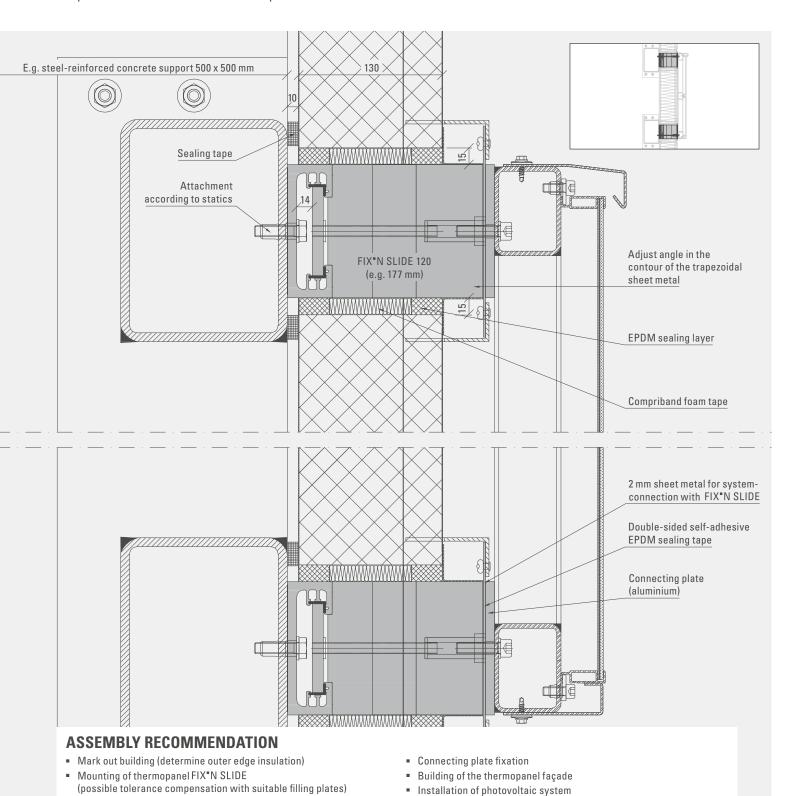




Photovoltaic modules on the substructure

Trapezoidal sheet metal thermopanel

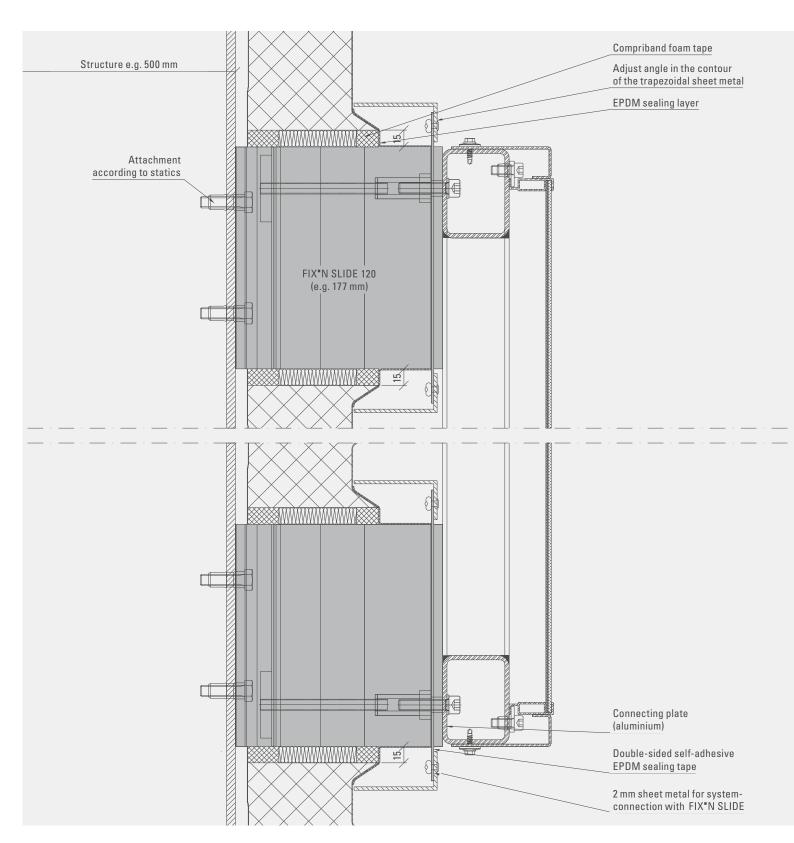
Vertical section



EPDM sealing tape

Establishment of the outer sealing using double-sided adhesive



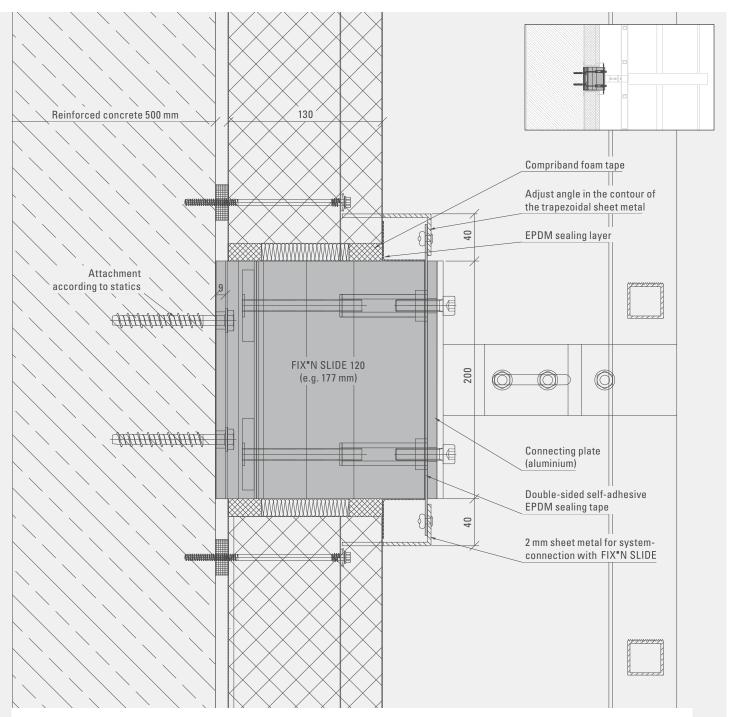




Fixed ladder DIN 18799-1

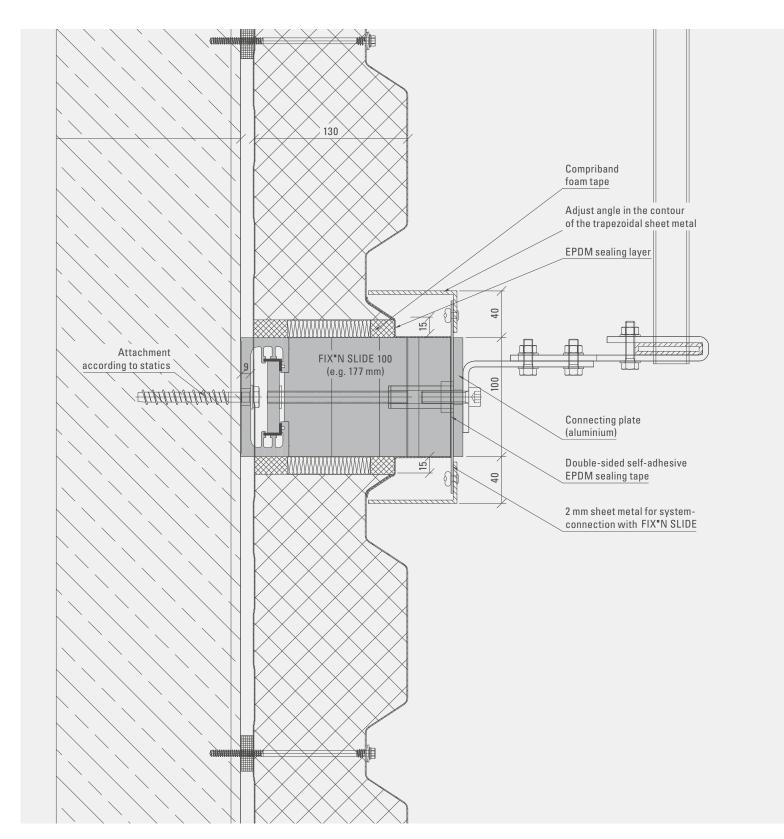
Trapezoidal sheet metal thermopanel

Vertical section

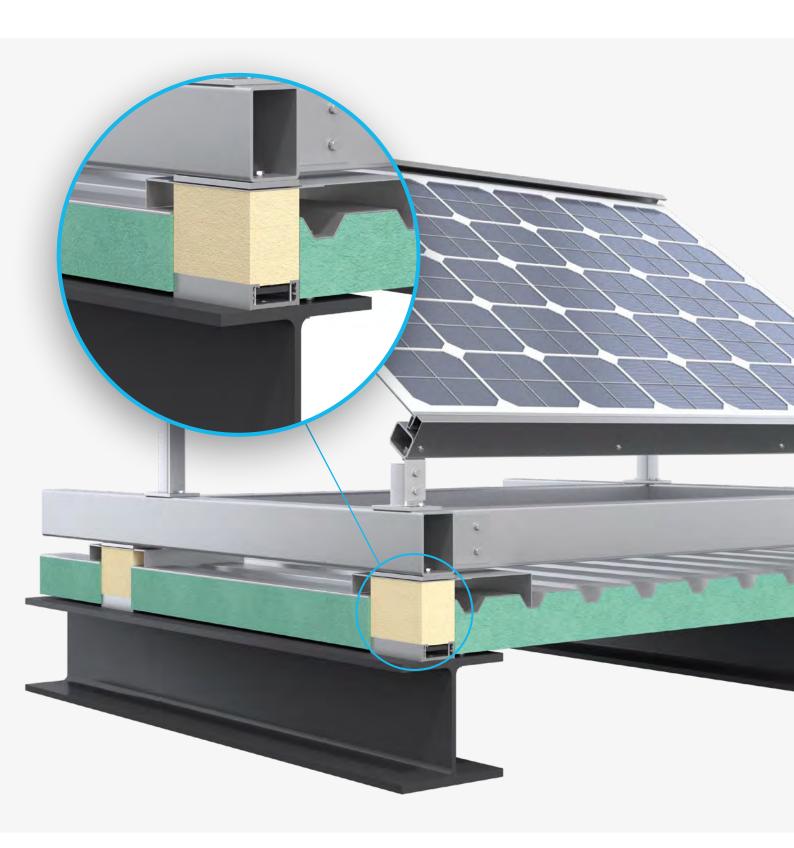


- Mark out building (determine outer edge insulation)
- Mounting of thermopanel FIX*N SLIDE (possible tolerance compensation with suitable filling plates)
- Establishment of the outer sealing using double-sided adhesive EPDM sealing tape
- Connecting plate fixation
- Building of the thermopanel façade
- Installation of vertical ladder











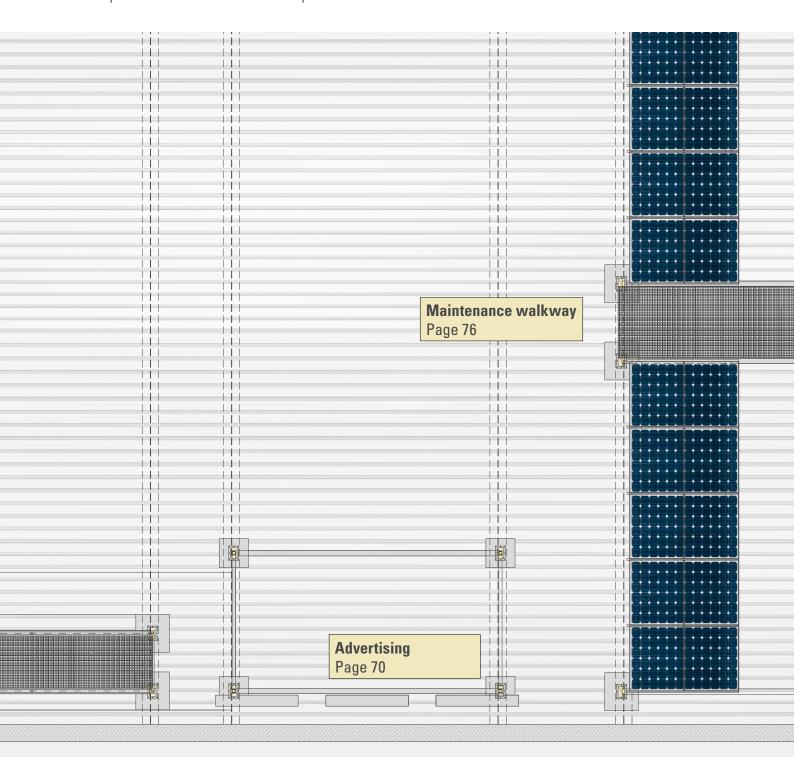
INDUSTRIAL HALL WITH ROOF THERMOPANEL AND PHOTOVOLTAIC MODULES

APPLICATION EXAMPLES

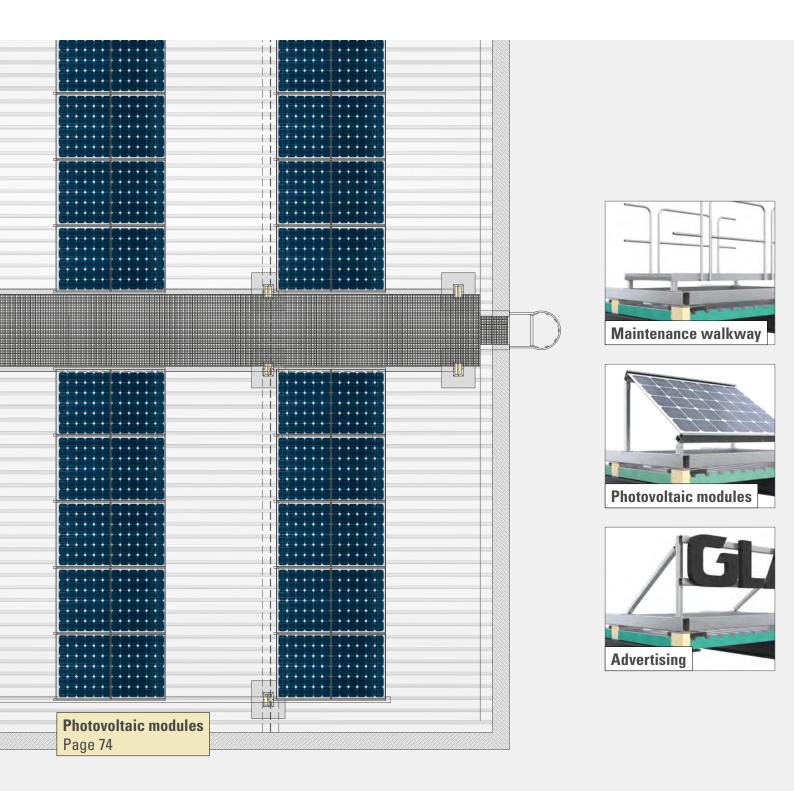


Top view of an industrial hall

with trapezoidal sheet metal thermopanel





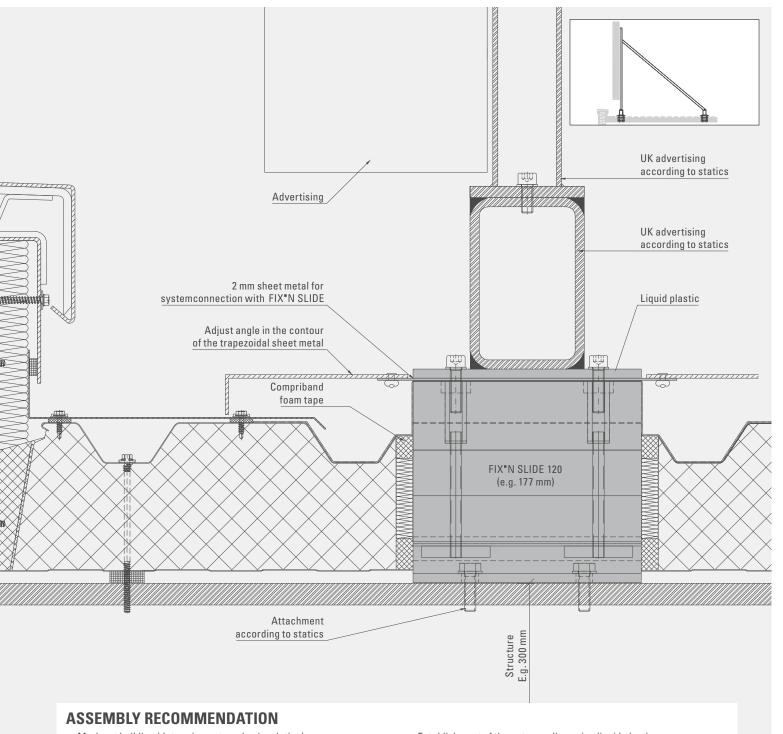




Advertising on an industrial hall

Trapezoidal sheet metal roof thermopanel

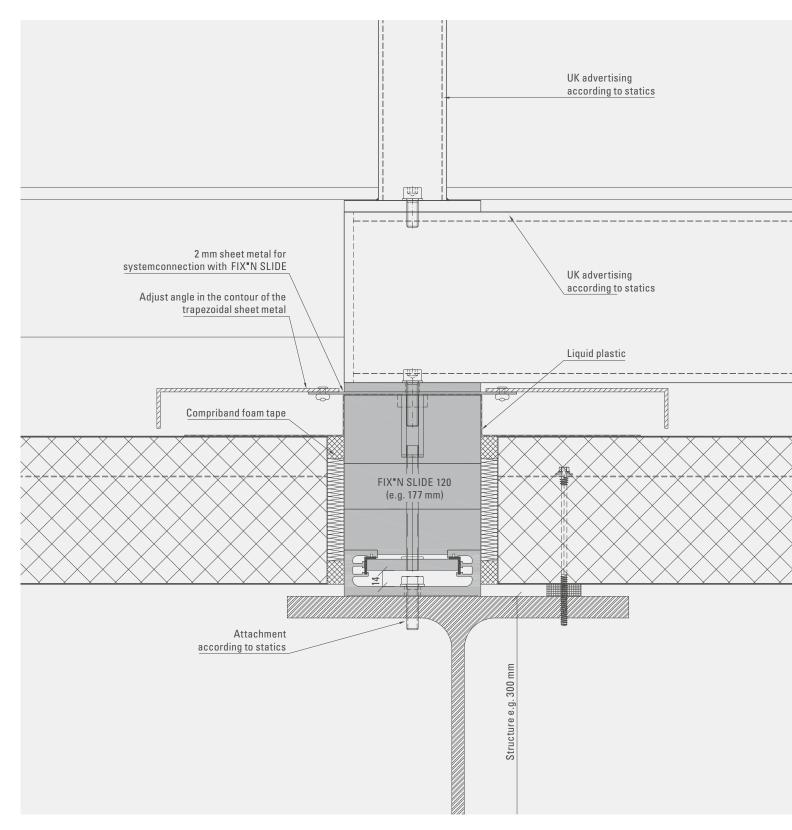
Vertical section



- Mark out building (determine outer edge insulation)
- Mounting of FIX*N SLIDE (possible tolerance compensation with suitable filling plates)
- Building of the roof thermopanel

- Establishment of the outer sealing using liquid plastic
- Connecting plate fixation
- Mounting of UK advertising



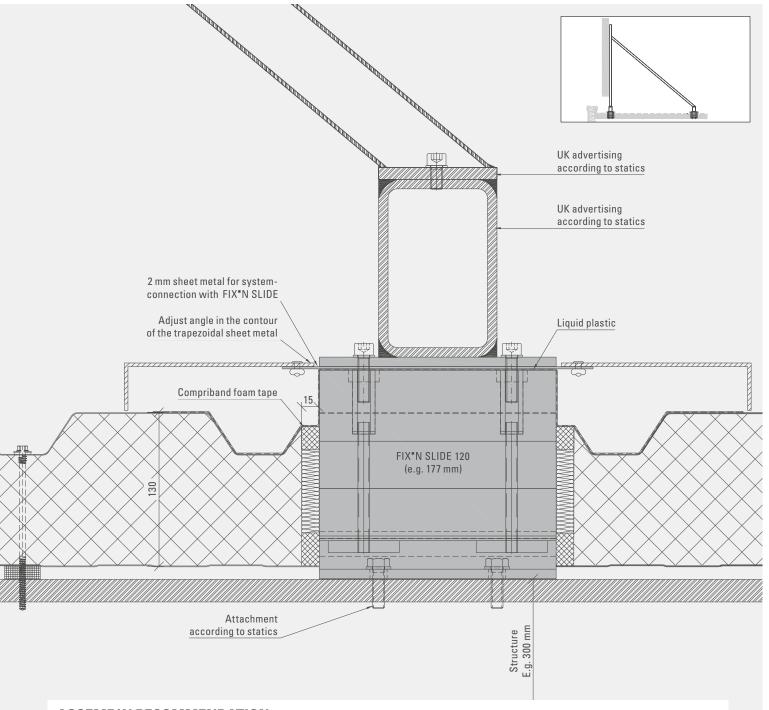




Advertising on an industrial hall

Trapezoidal sheet metal roof thermopanel

Vertical section

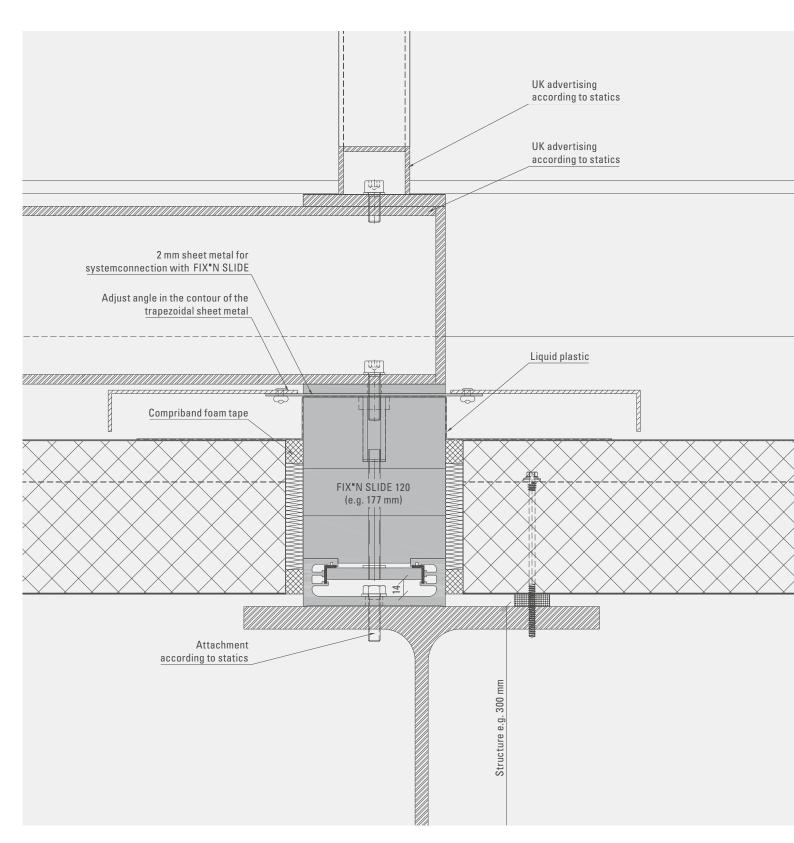


- Mark out building (determine outer edge insulation)
- Mounting of FIX*N SLIDE (possible tolerance compensation with suitable filling plates)
- Building of the roof thermopanel

- Establishment of the outer sealing using liquid plastic
- Connecting plate fixation
- Mounting of UK advertising



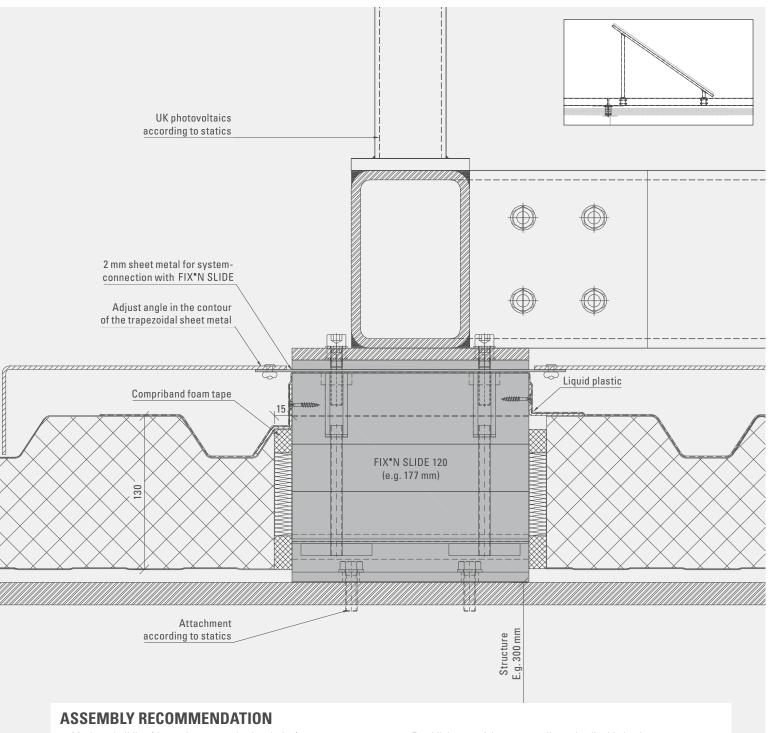
Horizontal section





Photovoltaic modules in the industrial hall

Substructure on roof Vertical section

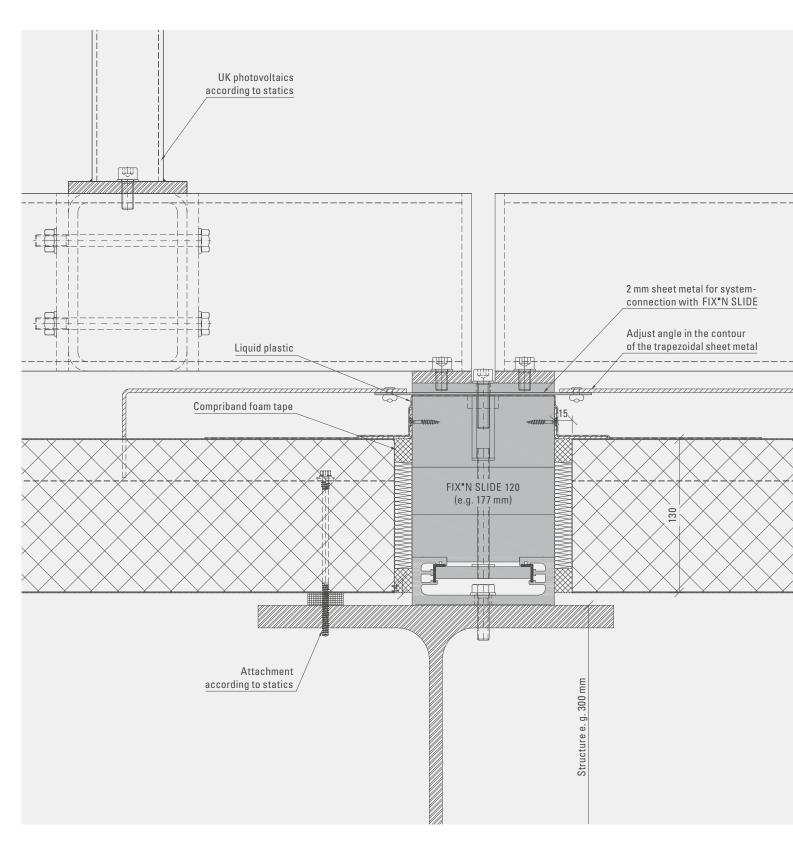


- Mark out building (determine outer edge insulation)
- Mounting of FIX*N SLIDE (possible tolerance compensation with suitable filling plates)
- Building of the roof thermopanel

- Establishment of the outer sealing using liquid plastic
- Connecting plate fixation
- Mounting of photovoltaic modules



Horizontal section

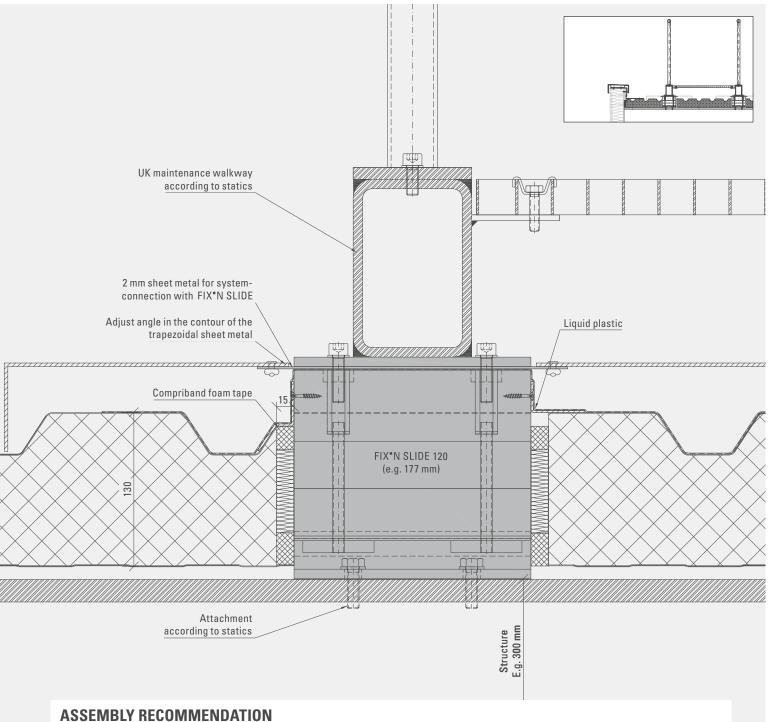




Maintenance walkway

Trapezoidal sheet metal roof thermopanel

Vertical section

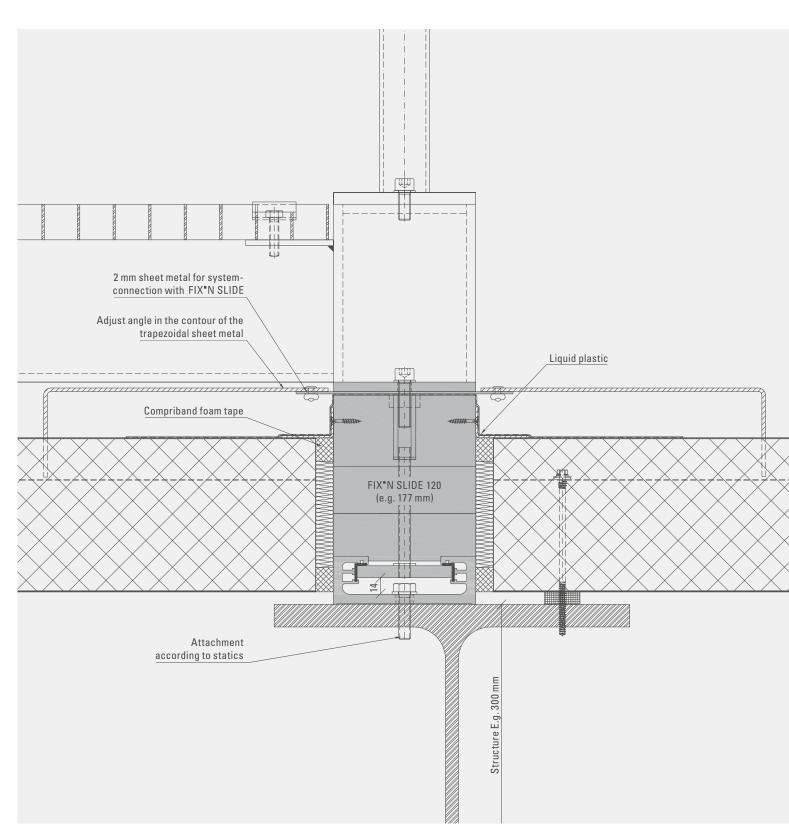


- Mark out building (determine outer edge insulation)
- Mounting of FIX"N SLIDE (possible tolerance compensation with suitable filling plates)
- Building of the roof thermopanel

- Establishment of the outer sealing using liquid plastic
- Connecting plate fixation
- Installation of maintenance walkway



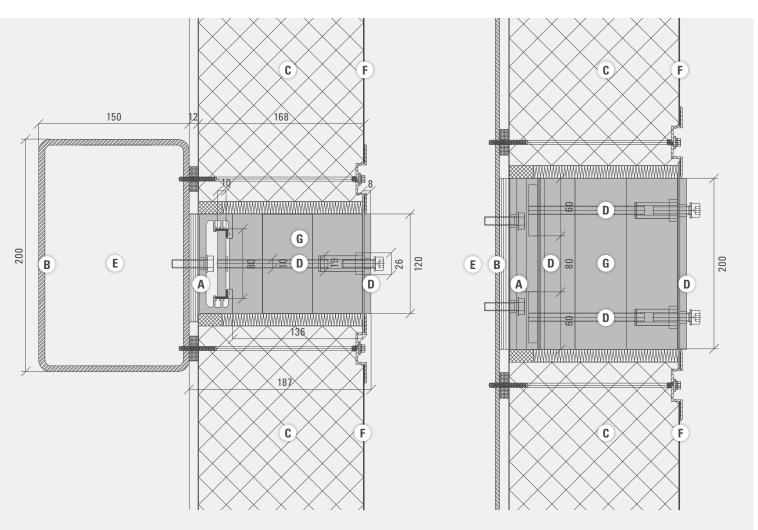
Horizontal section





THERMAL INSULATION CALCULATIONS

Point-to-point connection to smooth sheet metal according to DIN 4108-2 and χ value calculation (example)



Materials

		λ[W7(m•K)]	ε
A	Aluminium profile	160,000	0.900
В	Steel profile	50,000	0.900
C	Insulation WLG 035	0.035	0.900
D	Stainless steel	17,000	0.900
E	Air		
F	Aluminium	160,000	0.900
G	Pressure-resistant system insulating	material 0.083	0.900

Properties

Component (B x H x L)
 120 x 187 x 200 mm
 140 mm screw spacing



Boundary conditions

Temperatures

Exterior: $T_a = -5$ °C Interior: $T_i = 20$ °C

Heat transfer

Exterior: $R_a = 0.04 \text{ m}^2 \text{ K/W}$

Interior: $R_i = 0.13 \text{ m}^2 \text{K/W}$ (heat flow)

 $R_i = 0.25 \text{ m}^2 \text{K/W} \text{ (temperature)}$

 Thermal bridge surcharge for energy planning according to EnEV 2016

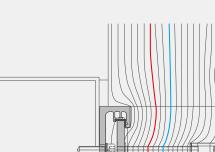
Xi value of the punctiform thermal bridge

= 0.032 W/K

Isothermal calculations

12.6°C isotherm

10.0°C isotherm



Results

• Minimum thermal insulation

 $f_{RSi} = 0.94 (>0.70)$

T = 18.52°C

Minumum thermal insulation met

- Wall structure U = 0.20 W/m²K
 150 mm Steel profile
 168 mm Insulation WLG 035
- Inspection report for the thermal simulation
 Inspection report no.
 FS_120_0200_PANL_170_P
- Excerpt from the relevant standards
 DIN 4108-2, DIN EN ISO 13788, DIN EN ISO
 10211, DIN EN ISO 10077, DIN EN ISO 12631
 DIN EN ISO 6946

Point-to-point connection

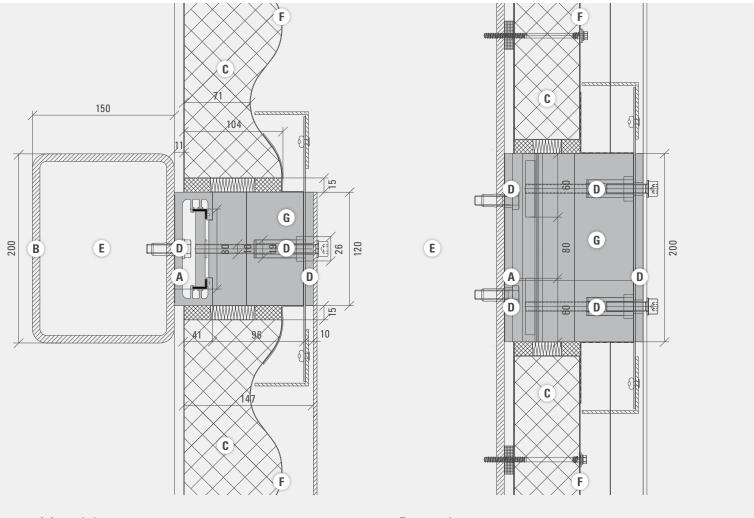
FIX'N SLIDE	Insulation thickness mm	Xi value W/K	f _{RSI} >0.70	T °C
120	168	0.032	0.940	18.52



THERMAL INSULATION CALCULATIONS

Point-to-point connection to thermal panel

according to DIN 4108-2 and ${\mathcal X}$ value calculation (example)



Materials

	λ	[W7(m•K)]	\mathcal{E}
A	Aluminium	160,000	0.900
B	Steel profile	50,000	0.900
C	Insulation WLG 035	0.035	0.900
D	Stainless steel	17,000	0.900
E	Air		
F	Aluminium profile	160,000	0.900
G	Pressure-resistant system insulating mate	erial 0.083	0.900

Properties

Component (B x H x L)
 120 x 147 x 200 mm
 140 mm screw spacing



Boundary conditions

Temperatures

Exterior: $T_a = -5$ °C Interior: $T_i = 20$ °C

Heat transfer

Exterior: $R_a = 0.04 \text{ m}^2 \text{ K/W}$

Interior: $R_i = 0.13 \text{ m}^2 \text{K/W}$ (heat flow)

 $R_i = 0.25 \text{ m}^2 \text{K/W} \text{ (temperature)}$

 Thermal bridge surcharge for energy planning according to EnEV 2016

Xi value of the punctiform thermal bridge = 0.052 W/K

Isothermal calculations

12.6°C isotherm

10.0°C isotherm



Results

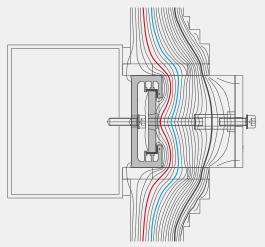
• Minimum thermal insulation

 $f_{RSi} = 0.890 (>0.70)$

T = 17.22°C

minimum thermal insulation met

- Wall structure U = 0.20 W/m²K
 150 mm Steel profile
 104 mm Insulation WLG 035
- Inspection report for the thermal simulation
 Inspection report no.
 FS_120_0200_ISOW_104_P
- Excerpt from the relevant standards
 DIN 4108-2, DIN EN ISO 13788, DIN EN ISO
 10211, DIN EN ISO 10077, DIN EN ISO 12631
 DIN EN ISO 6946



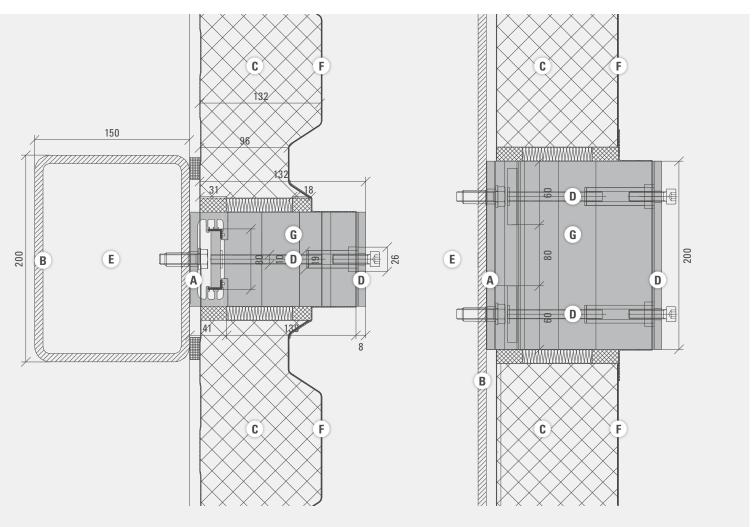
Point-to-point connection

FIX'N SLIDE	Insulation thickness mm	Xi value W/K	f _{RSI} >0.70	T °C
120	104	0.052	0.890	17.22



THERMAL INSULATION CALCULATIONS

Point-to-point connection to trapezoidal sheet metal according to DIN 4108-2 and χ value calculation (example)



Materials

		λ[W7(m•K)]	ε
A	Aluminium profile	160,000	0.900
В	Steel profile	50,000	0.900
C	Insulation WLG 035	0.035	0.900
D	Stainless steel	17,000	0.900
E	Air		
F	Aluminium	160,000	0.900

G Pressure-resistant system insulating material 0.083

0.900

Properties

Component (B x H x L)120 x 132 x 200 mm140 mm screw spacing



Boundary conditions

Temperatures

Exterior: $T_a = -5$ °C Interior: $T_i = 20$ °C

Heat transfer

Exterior: $R_a = 0.04 \text{ m}^2 \text{ K/W}$

Interior: $R_i = 0.13 \text{ m}^2 \text{K/W}$ (heat flow)

 $R_i = 0.25 \text{ m}^2 \text{K/W} \text{ (temperature)}$

 Thermal bridge surcharge for energy planning according to EnEV 2016

Xi value of the punctiform thermal bridge

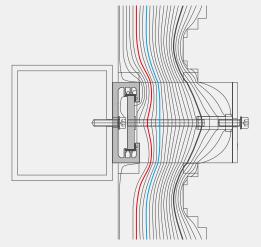
= 0.035 W/K

Isothermal calculations

12.6°C isotherm

10.0°C isotherm





Results

Minimum thermal insulation

 $f_{RSi} = 0.93 (>0.70)$

T = 18.16° C

Minimum thermal insulation met

- Wall structure U = 0.20 W/m²K
 150 mm Steel profile
 132 mm Insulation WLG 035
- Inspection report for the thermal simulation
 Inspection report no.
 FS_120_0200_TRPZ_132_P
- Excerpt from the relevant standards
 DIN 4108-2, DIN EN ISO 13788, DIN EN ISO
 10211, DIN EN ISO 10077, DIN EN ISO 12631
 DIN EN ISO 6946

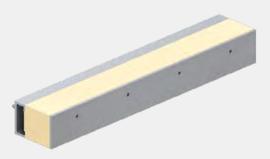
Point-to-point connection

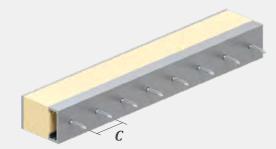
FIX'N SLIDE	Insulation thickness	Xi value	f _{RSI}	T
	mm	W/K	>0.70	°C
120	132	0.035	0.930	18.14



DIMENSIONS

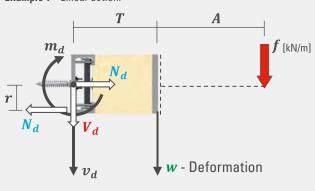
Linear connection (action perpendicular to element axis)



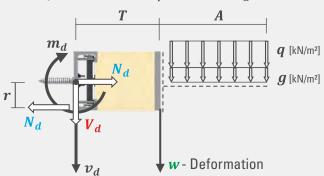


Actions/effects

Example 1 – Linear action:



Example 2 – Distributed load (q) and dead weight (q):



Bearing capacity limit state

$$m_d \le m_{R.d}$$
 and $v_d \le v_{R.d}$

Calculated values of the linear bearing torques m_d and the linear bearing forces v_d :

Example 1

$$\begin{aligned} v_{d \text{ [kN/m]}} &= \gamma_{Q} \cdot f_{\text{ [kN/m]}} \\ m_{d \text{ [kNm/m]}} &= v_{d \text{ [kN/m]}} \cdot (T_{\text{[m]}} + A_{\text{[m]}}) \end{aligned}$$

Example 2

$$v_{d \text{ [kN/m]}} = (\gamma_Q \cdot q_{k \text{ [kN/m^2]}} + \gamma_G \cdot g_{\text{ [kN/m^2]}}) \cdot A_{\text{ [m]}}$$

$$m_{d \text{ [kNm/m]}} = v_{d \text{ [kN/m]}} \cdot (T_{\text{ [m]}} + A_{\text{ [m]}}/2)$$

	T [mm]	Up to 90	90-100	100-120	120-140	140-160	160-180	180-200	200-220	220-240	240-260	260-280	280-300	300-320
FS 48	$m_{R.d}$ [kNm/m]	0.76	0.72	0.66	0.6	0.56	0.53	0.50	0.48	0.46	0.44	0.42	0.41	0.39
F3 40	$v_{R.d}$ [kN/m]	8.5	7.2	5.5	4.3	3.5	3.0	2.5	2.2	1.9	1.7	1.5	1.4	1.3
FS 60	$m_{R.d}$ [kNm/m]	1.00	1.32	1.20	1.11	1.04	0.98	0.93	0.88	0.85	0.81	0.78	0.75	0.73
L2 00	$v_{R.d}$ [kN/m]	15.5	13.2	10.0	8.0	6.5	5.5	4.7	4.0	3.6	3.2	2.8	2.5	2.3
FS 80	$m_{R.d}$ [kNm/m]	2.77	2.55	2.20	1.95	1.75	1.59	1.46	1.35	1.26	1.18	1.12	1.06	1.00
L2 00	$v_{R.d}$ [kN/m]	30.8	25.5	18.4	13.9	10.9	8.9	7.3	6.2	5.3	4.6	4.0	3.6	3.2
FS 100	$m_{R.d}$ [kNm/m]	4.24	3.98	3.56	3.25	2.99	2.79	2.62	2.47	2.34	2.23	2.14	2.05	1.97
F3 100	$v_{R.d}$ [kN/m]	47.1	39.8	29.7	23.2	18.7	15.5	13.1	11.3	9.8	8.6	7.7	6.9	6.2
FS 120	$m_{R.d}$ [kNm/m]	7.76	7.19	6.31	5.65	5.14	4.72	4.38	4.09	3.84	3.63	3.44	3.28	3.13
F3 120	$v_{R.d}$ [kN/m]	52.4	52.4	52.4	40.4	32.1	26.3	21.9	18.6	16.0	14.0	12.3	11.0	9.8

The values $m_{R,d}$ and $v_{R,d}$ in the above table apply to permanent and temporary design situations with short and/or medium load durations (such as the action of wind, snow or traffic loads and their combinations with the attachment weight). In load situations with predominantly permanent actions (such as only the action of the attachment weight), the values $m_{R,d}$ and $v_{R,d}$ from the above table are to be multiplied with a reduction factor of 0.75. If consideration is to be given to dynamic, multiaxial or other special actions, or actions that may result from unfavourable external influences (such as in exposed installations), a separate analysis needs to be done.



Serviceability limit state (deformation)

Characteristic values of the linear bearing torques $m{m}$:

Example 1 – Linear action:

Example 2 – distributed load and dead weight:

$$m_{\text{[kNm/m]}} = f_{\text{[kN/m]}} \cdot (T_{\text{[m]}} + A_{\text{[m]}})$$

$$m_{\text{[kNm/m]}} = (q_{\text{[kN/m^2]}} + g_{\text{[kN/m^2]}}) \cdot A_{\text{[m]}} \cdot (T_{\text{[m]}} + A_{\text{[m]}}/2)$$

Existing deformation w on the front edge of the FS element subject to the element depth T and the characteristic linear torque m:

	T [mm]	Up to 90	90-100	100-120	120-140	140-160	160-180	180-200	200-220	220-240	240-260	260-280	280-300	300-320
	m [kNm/m]					E	kisting de	eformatio	on w (mn	1]*				
	Up to 0.20	< 1	< 1	2	3	3	3	4	4	5	5	5	5	5
FS 48	0.20 - 0.25	< 1	< 1	2	3	3								
	0.25 - 0.30	< 1	< 1	2	3	3								
	Up to 0.20	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	2	2
	0.20 - 0.30	< 1	< 1	< 1	< 1	< 1	2	2	2	2	3	3	3	4
FS 60	0.30 - 0.40	< 1	< 1	< 1	2	2	2	3	3	4	4			
	0.40 - 0.50	< 1	< 1	< 1	2	3	3	4						
	0.50 - 0.60	< 1	< 1	2	3	3	4		-					
	Up to 0.20	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	2	2
	0.20 - 0.40	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	2	2	3	4
FS 80	0.40 - 0.60	< 1	< 1	< 1	< 1	< 1	< 1	< 1	2	3	3	4		
L9 90	0.60 - 0.80	< 1	< 1	< 1	< 1	< 1	2	2	3	4	5			
	0.80 - 1.00	< 1	< 1	< 1	< 1	2	3	3	4			•		
	1.00 - 1.20	< 1	< 1	< 1	2	3	3							
	Up to 0.25	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	2	2
	0.25 - 0.50	< 1	< 1	< 1	< 1	< 1	< 1	< 1	2	2	2	2	2	3
	0.50 - 0.75	< 1	< 1	< 1	< 1	< 1	< 1	2	2	2	3	3	4	4
FS 100	0.75 - 1.00	< 1	< 1	< 1	< 1	< 1	< 1	2	2	3	3	4	5	5
	1.00 - 1.25	< 1	< 1	< 1	< 1	2	2	2	3	3	4			
	1.25 - 1.50	< 1	< 1	< 1	< 1	2	2	2	3	4				
	1.50 - 1.75	< 1	< 1	< 1	< 1	2	2	3	4					
	Up to 1.00	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	2	2	2	2	3
	1.00 - 1.25	< 1	< 1	< 1	< 1	< 1	< 1	2	2	2	2	3	3	4
	1.25 - 1.75	< 1	< 1	< 1	< 1	< 1	< 1	2	2	3	3	4	4	5
FS 120	1.75 - 2.00	< 1	< 1	< 1	< 1	< 1	2	2	3	3	4	4	5	6
	2.00 - 2.25	< 1	< 1	< 1	<1	2	2	2	3	4	4	5	6	
	2.25 - 2.75	< 1	< 1	< 1	< 1	2	2	3	3	4				
	2.75 - 3.25	<1	< 1	< 1	< 1	2	2	3	4					

^{*} In installations that are especially sensitive to deformation and installations under high sustained loads, the use of a larger FS element is recommended. The values are the expected deformation. The influence of the rigidity of the substructure is not taken into account.

Bearing forces:	N_{d} [kN]	= $m_{d \text{ [kNm/m]}}$ ·	$oldsymbol{c}_{\scriptscriptstyle [m]}$ / $oldsymbol{r}_{\scriptscriptstyle [m]}$	$V_{d \text{ [kN]}} =$	$v_{d_{[kNm/m]}} \cdot c_{_{[m]}}$	<i>C</i> = E.g. 0.1 m
	FS 48	FS 60	FS 80	FS 100	FS 120	
$oldsymbol{r}_{\scriptscriptstyle [m]}$	0.023	0.028	0.038	0.047	0.057	

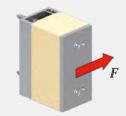
 $Verifications \ of load \ application \ and \ transfer, \ as \ well \ as \ of the \ substructure, \ are \ not \ recorded \ or \ produced \ together \ with \ the \ verifications \ of \ the \ FS \ elements.$



DIMENSIONS

Point-to-point connection (action perpendicular to element axis)

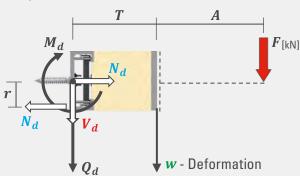






Actions/effects

Example – Individual load:



Bearing capacity limit state $M_d \le M_{R,d}$ and $Q_d \le Q_{R,d}$

Calculated values of the bearing torques $oldsymbol{M_d}$ and the bearing forces $oldsymbol{Q_d}$ per 200 mm element:

$$\begin{aligned} & \boldsymbol{Q_{d}}_{\text{[kN]}} = & \boldsymbol{\gamma_{Q}} \cdot \boldsymbol{F}_{\text{[kN]}} \\ & \boldsymbol{M_{d}}_{\text{[kNm]}} = & \boldsymbol{Q_{d}}_{\text{[kN]}} \cdot (\boldsymbol{T}_{\text{[m]}} + \boldsymbol{A}_{\text{[m]}}) \end{aligned}$$

	T [mm]	Up to 90	90-100	100-120	120-140	140-160	160-180	180-200	200-220	220-240	240-260	260-280	280-300	300-320
FS 48	$M_{R.d}$ [kNm]	0.26	0.25	0.23	0.22	0.20	0.19	0.18	0.18	0.17	0.16	0.16	0.16	0.15
F3 40	$oldsymbol{Q}_{R.d}\left[kN ight]$	1.9	1.9	1.9	1.6	1.3	1.1	0.9	0.8	0.7	0.7	0.6	0.6	0.5
FS 60	$M_{R.d}$ [kNm]	0.35	0.34	0.32	0.3	0.29	0.28	0.27	0.26	0.26	0.25	0.24	0.24	0.23
L2 00	$Q_{R.d}$ [kN]	3.9	3.4	2.7	2.2	1.8	1.6	1.4	1.2	1.1	1.0	0.9	0.8	0.8
FS 80	$M_{R.d}$ [kNm]	0.74	0.70	0.65	0.60	0.57	0.54	0.51	0.49	0.47	0.45	0.44	0.43	0.41
L2 00	$Q_{R.d}$ [kN]	7.6	7.0	5.4	4.3	3.6	3.0	2.6	2.3	2.0	1.8	1.6	1.5	1.3
FS 100	$M_{R.d}$ [kNm]	1.32	1.26	1.16	1.08	1.01	0.96	0.91	0.87	0.84	0.81	0.78	0.76	0.74
13 100	$oldsymbol{Q}_{R.d}$ [kN]	10.5	10.5	8.5	6.9	5.8	5.0	4.3	3.8	3.4	3.1	2.8	2.6	2.4
FS 120	$M_{R.d}$ [kNm]	1.88	1.81	1.70	1.61	1.54	1.48	1.42	1.38	1.34	1.30	1.27	1.24	1.21
F3 120	$Q_{R.d}$ [kN]	10.5	10.5	10.5	10.5	9.1	7.8	6.9	6.1	5.5	4.9	4.5	4.1	3.8

The values $M_{R,d}$ and $Q_{R,d}$ in the above table apply to permanent and temporary design situations with short and/or medium load durations (such as the action of wind, snow or traffic loads and their combinations with the attachment weight). In load situations with predominantly permanent actions (such as only the action of the attachment weight), the values $M_{R,d}$ and $Q_{R,d}$ from the above table are to be multiplied with a reduction factor of 0.75. If consideration is to be given to dynamic, multiaxial or other special actions, or actions that may result from unfavourable external influences (such as in exposed installations), a separate analysis needs to be done.



Serviceability limit state (deformation)

Characteristic values of the linear bearing torques ${\it M}$:

$$M_{\text{[kNm]}} = F_{\text{[kN]}} \cdot (T_{\text{[m]}} + A_{\text{[m]}})$$

Existing deformation \boldsymbol{w} on the front edge of the FS element subject to the element depth \boldsymbol{T} and the characteristic linear torque \boldsymbol{M} :

	<i>T</i> [mm]	Up to 90	90-100	100-120	120-140	140-160	160-180	180-200	200-220	220-240	240-260	260-280	280-300	300-320
	M [kNm]					E	kisting de	eformatio	on w [mm	1]*				
	Up to 0.05	< 1	< 1	< 1	< 1	< 1	2	2	3	3	3	3	3	4
FS 48	0.05 - 0.10	< 1	< 1	< 1	2	2								
	0.10 - 0.15	< 1	2	2										
	Up to 0.05	< 1	< 1	< 1	< 1	< 1	< 1	< 1	2	2	2	2	2	2
FS 60	0.05 - 0.10	< 1	< 1	< 1	2	2	2	3	3	3	4	4	5	5
13 00	0.10 - 0.15	< 1	< 1	2	2	3	4	4						
	0.15 - 0.20	< 1	2									,		
	Up to 0.05	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	2	2
	0.05 - 0.10	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	2	2	2	3
FS 80	0.10 - 0.20	< 1	< 1	< 1	< 1	< 1	< 1	2	2	3	3	4	5	5
	0.20 - 0.30	< 1	< 1	< 1	2	2	3	3	4					
	0.30 - 0.40	< 1	< 1	2	3	3								
	Up to 0.10	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1
	0.10 - 0.20	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	2	2	2	2	3
FS 100	0.20 - 0.30	< 1	< 1	< 1	< 1	2	2	2	3	3	3	4	4	5
13 100	0.30 - 0.40	< 1	< 1	< 1	2	3	3	4						
	0.40 - 0.50	< 1	< 1	2										
	0.50 - 0.60	< 1	< 1											
	Up to 0.40	< 1	< 1	< 1	< 1	< 1	< 1	2	2	2	2	3	3	3
	0.40 - 0.50	< 1	< 1	< 1	< 1	2	2	2	2	3	3	4	4	4
	0.50 - 0.60	< 1	< 1	< 1	< 1	2	2	3	3	4	4	5	5	6
FS 120	0.60 - 0.70	< 1	< 1	< 1	2	2	3	3	4	5	5			
	0.70 - 0.80	< 1	< 1	< 1	2	3	3	4						
	0.80 - 0.90	< 1	< 1	2	2									
	0.90 - 1.00	< 1	< 1	2										

^{*} In installations that are especially sensitive to deformation and installations under high sustained loads, the use of a larger FS element is recommended. The values are the expected deformation. The influence of the rigidity of the substructure is not taken into account.

Bearing forces per connection (dowel/screw): $N_{d_{[kN]}} = M_{d_{[kN]}} / (r_{[m]} \cdot 2)$ $V_{d_{[kN]}} = Q_{d_{[kN]}} / 2$

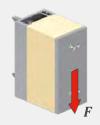
	FS 48	FS 60	FS 80	FS 100	FS 120
$oldsymbol{r}_{ iny{fm}}$	0.023	0.028	0.038	0.047	0.057

Verifications of load application and transfer, as well as of the substructure, are not recorded or produced together with the verifications of the FS elements.

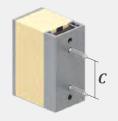


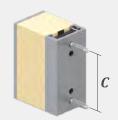
DIMENSIONS

Point-to-point connection (action perpendicular to element axis)





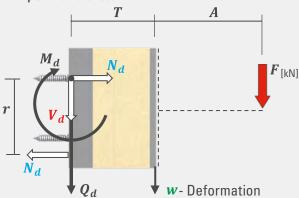




 $C = 100 - 150 \, \text{mm}$

Actions/effects

Example – Individual load:



Bearing capacity limit state

$$M_d \le M_{R,d}$$
 and $Q_d \le Q_{R,d}$

Calculated values of the bearing torques $m{M}_d$ and the bearing forces $m{Q}_d$ per 200 mm element:

$$\begin{aligned} & \boldsymbol{Q_{d}}_{\text{[kN]}} = & \boldsymbol{\gamma_{Q}} \cdot \boldsymbol{F}_{\text{[kN]}} \\ & \boldsymbol{M_{d}}_{\text{[kNm]}} = & \boldsymbol{Q_{d}}_{\text{[kN]}} \cdot (\boldsymbol{T}_{\text{[m]}} + \boldsymbol{A}_{\text{[m]}}) \end{aligned}$$

	T [mm]	Up to 90	90-100	100-120	120-140	140-160	160-180	180-200	200-220	220-240	240-260	260-280	280-300	300-320
FS 48	$M_{R.d}$ [kNm]	1.10	1.07	1.01	0.96	0.92	0.89	0.86	0.83	0.81	0.79	0.77	0.75	0.74
F3 40	$oldsymbol{Q}_{R.d}\left[kN ight]$	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2
FS 60	$M_{R.d}$ [kNm]	1.78	1.72	1.63	1.55	1.49	1.44	1.39	1.35	1.31	1.28	1.25	1.23	1.20
L2 00	$oldsymbol{Q}_{R.d}$ [kN]	3.3	3.3	3.3	3.3	3.3	3.3	3.3	3.3	3.3	3.3	3.3	3.3	3.3
FS 80	$M_{R.d}$ [kNm]	1.48	1.44	1.37	1.31	1.26	1.22	1.19	1.16	1.13	1.10	1.08	1.06	1.04
L9 00	$oldsymbol{Q}_{R.d}$ [kN]	3.4	3.4	3.4	3.4	3.4	3.4	3.4	3.4	3.4	3.4	3.4	3.4	3.3
FS 100	$M_{R.d}$ [kNm]	3.61	3.36	2.97	2.67	2.44	2.25	2.10	1.96	1.85	1.75	1.67	1.59	1.52
F3 100	$oldsymbol{Q}_{R.d}$ [kN]	4.5	4.5	4.5	4.5	4.5	4.5	4.5	4.5	4.5	4.5	4.5	4.5	4.5
FS 120	$oldsymbol{M}_{R.d}$ [kNm]	2.85	2.66	2.35	2.12	1.94	1.80	1.67	1.57	1.48	1.41	1.34	1.28	1.22
F3 120	$oldsymbol{Q}_{R.d}\left[kN ight]$	4.5	4.5	4.5	4.5	4.5	4.5	4.5	4.5	4.5	4.5	4.5	4.3	3.9

The values $M_{R,d}$ and $Q_{R,d}$ in the above table apply to permanent and temporary design situations with short and/or medium load durations (such as the action of wind, snow or traffic loads and their combinations with the attachment weight). In load situations with predominantly permanent actions (such as only the action of the attachment weight), the values $M_{R,d}$ and $Q_{R,d}$ from the above table are to be multiplied with a reduction factor of 0.75. If consideration is to be given to dynamic, multiaxial or other special actions, or actions that may result from unfavourable external influences (such as in exposed installations), a separate analysis needs to be done.



Serviceability limit state (deformation)

Characteristic values of the linear bearing torques ${\it M}$:

$$\boldsymbol{M}_{[kNm]} = \boldsymbol{F}_{[kN]} \cdot (\boldsymbol{T}_{[m]} + \boldsymbol{A}_{[m]})$$

Existing deformation \boldsymbol{w} on the front edge of the FS element subject to the element depth \boldsymbol{T} and the characteristic linear torque \boldsymbol{M} :

	T [mm]	Up to 90	90-100	100-120	120-140	140-160	160-180	180-200	200-220	220-240	240-260	260-280	280-300	300-320
	M [kNm]		Existing deformation w [mm]*											
	Up to 0.20	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1
	0.20 - 0.30	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1
FS 48	0.30 - 0.40	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	2	2
	0.40 - 0.50	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	2	2	2	2	2
	0.50 - 0.60	< 1	< 1	< 1	< 1	< 1	< 1	2	2	2	2	3	3	3
	Up to 0.30	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1
	0.30 - 0.40	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1
	0.40 - 0.50	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1
FS 60	0.50 - 0.60	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1
	0.60 - 0.70	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1
	0.70 - 0.80	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	2	2	2
	0.80 - 0.90	< 1	< 1	< 1	< 1	< 1	< 1	< 1	2	2	2	2	2	3
	Up to 0.30	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1
	0.30 - 0.40	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1
	0.40 - 0.50	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	2
FS 80	0.50 - 0.60	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	2	2	2
	0.60 - 0.70	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	2	2	2	2	2
	0.70 - 0.80	< 1	< 1	< 1	< 1	< 1	< 1	2	2	2	2	2	3	3
	0.80 - 0.90	< 1	< 1	< 1	< 1	< 1	2	2	2	2	3	3	3	4
	Up to 0.50	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1
	0.50 - 0.75	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	2	2	2
FS 100	0.75 - 1.00	< 1	< 1	< 1	< 1	< 1	< 1	< 1	2	2	2	2	2	2
	1.00 - 1.25	< 1	< 1	< 1	< 1	2	2	2	2	2	3	3	3	3
	1.25 - 1.50	< 1	< 1	< 1	2	2	2	2	3	3	3	4	4	4
	Up to 0.50	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1
	0.50 - 0.75	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	2	2	2
FS 120	0.75 - 1.00	< 1	< 1	< 1	< 1	< 1	< 1	< 1	2	2	2	2	2	3
	1.00 - 1.25	< 1	<1	< 1	< 1	<1	2	2	2	2	3	3	3	4
	1.25 - 1.50	<1	< 1	< 1	2	2	2	2	3	3	4	4	5	5

^{*} In installations that are especially sensitive to deformation and installations under high sustained loads, the use of a larger FS element is recommended. The values are the expected deformation. The influence of the rigidity of the substructure is not taken into account.

Bearing forces per connection (dowel/screw): $N_{d_{[kN]}} = M_{d_{[kN]}} / r_{[m]}$ $V_{d_{[kN]}} = Q_{d_{[kN]}} / 2$

	Where <i>C</i> = 100 mm						Where <i>C</i> = 150 mm					
	FS 48	FS 60	FS 80	FS 100	FS 120	FS 48	FS 60	FS 80	FS 100	FS 120		
$r_{\scriptscriptstyle [m]}$	0.135	0.137	0.140	0.143	0.144	0.158	0.159	0.161	0.162	0.163		

 $Verifications \ of load \ application \ and \ transfer, \ as \ well \ as \ of \ the \ SD \ elements.$



ASSEMBLY INSTRUCTIONS LINEAR CONNECTION



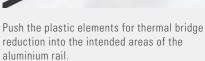
reduction into the intended areas of the



Determine the attachment points with the aid of the assembly rail. Attach the aluminium rail to the structure or structure with regulated/ approved fasteners.



Screw the tensile threaded rods into the slide-in plates and guide the slide-in plates into the aluminium rail.





Straighten the slide-in plates according to the attachment points of the add-on element by shifting them. Fasten the slide-in plates with the pre-drilled mounting aids.

5

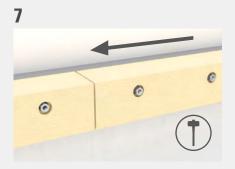


Push the pre-drilled insulating element over the threaded rods.

6



Guide the washers and threaded sockets up to the threaded rods and fasten these with a tightening torque of 10 Nm.



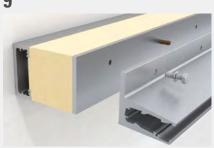
After attaching the first block, push the remaining blocks firmly together without gaps (optionally tap with a hammer).

8



Stick a bolt for mounting support into a threaded socket and stick the optional aluminium connecting plate with self-adhesive EPDM tape to the insulating element.

9



Adjust the add-on element (here the GLASSLINE CANOPY CLOUD) using the bolt and fasten it to the substructure with regulated/approved fasteners using a tightening torque of 24 Nm for M10 or 12 Nm for M8.

All screw connections are to be secured against loosening using suitable means.



ASSEMBLY INSTRUCTIONS

POINT-TO-POINT CONNECTION



Determine the attachment points with the aid of the U profile. Attach the U profile to the structure or structure with regulated/ approved fasteners.

2



Screw the tensile threaded rods into the slide-in plates.

3



Guide the slide-in plates into the aluminium rail.

4



Straighten the slide-in plates by shifting these to the pre-drilled mounting aid and fasten them.

5



Push the pre-drilled insulating element over the threaded rods.

6



Guide the washers and threaded sockets up to the threaded rods and fasten these with a tightening torque of 10 Nm.

7



Mount an adaptor plate with regulated/ approved fasteners using a tightening torque of 24 Nm for M10 or 12 Nm for M8.

Assembly video Linear connection



www.glassline.de/fs-linear

Assembly video Point-to-point connection



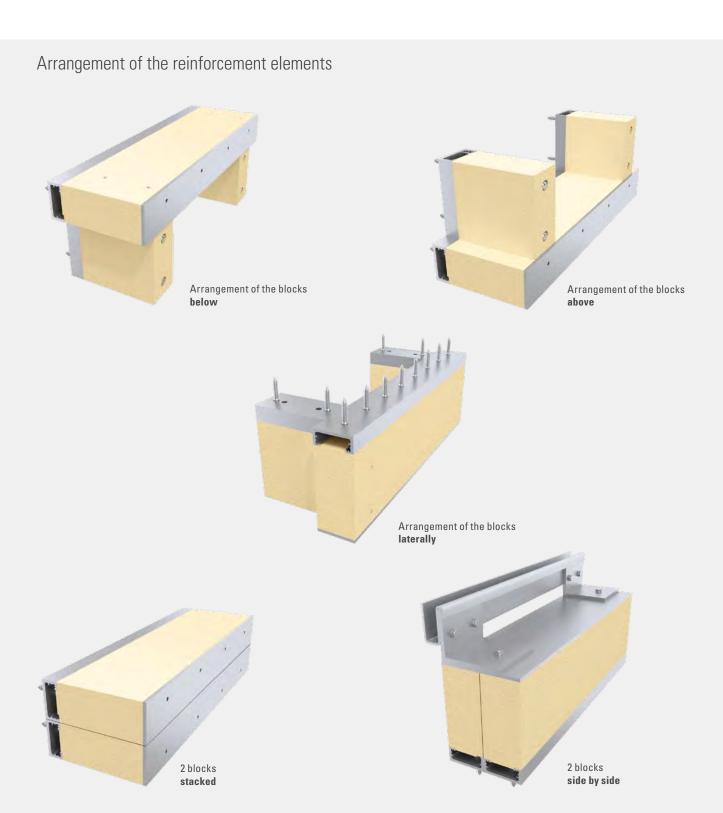
www.glassline.de/fs-point-to-point

All screw connections are to be secured against loosening using suitable means.



SOLUTIONS FOR REINFORCEMENT

With FIX N SLIDE

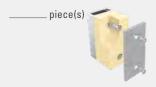


PRODUCT ENQUIRY FIX'N SLIDE

Your enquiry will be answered Name as soon as possible. Company Street/house number Construction project Postcode/city Telephone Telefax Email (Please fill out all fields)

FIX*N SLIDE

□ POINT-TO-POINT CONNECTION



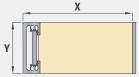
□ Optional adaptor plate (stainless steel)

□ LINEAR CONNECTION



□ Optional connecting plate (aluminium, surface E6/EV1)

BLOCK HEIGHTS



Sizes Y: □ 48 □ 60 □ 80 □ 100 □ 120

Special heights on request



□ 70 □ 80 □ 100 □ 120 □ 140 □ 160 □ 180 □ 200 □ 220 □ 240 □ 260

□ 280

□ 300

Block heights X:

Quick enquiry:

Fax to +49 (0) 6291/6259-11 or email to info@glassline.de

Print/save enquiry

Fill out

OU	+ 00	100	J + 12
	55		65
	75		85
	85		95
	105		115
	125		135
	145		155
	165		175
	185		195
	205		215
	225		235
	245		255
	265		275
	285		295

LINEAR CONNECTION



Lengths Z:

- □ 600 mm □ 800 mm
- □ 2.000 mm
- □ 1,200 mm
- □ 2,400 mm
- □ 1,400 mm
- □ 2,800 mm □ 3,000 mm
- □ 1,600 mm
- Special lengths on request

FIX*N SLIDE FOR CANOPY CLOUD STOCK PROGRAMME

CANOPY CLOUD PROFILE TYPE 1



Lengths:

- 1,400 mm piece(s)
- 1,600 mm piece(s)
- 2,000 mm piece(s)
- 2,400 mm. piece(s)

CANOPY CLOUD PROFILE TYPE 3

□ 315



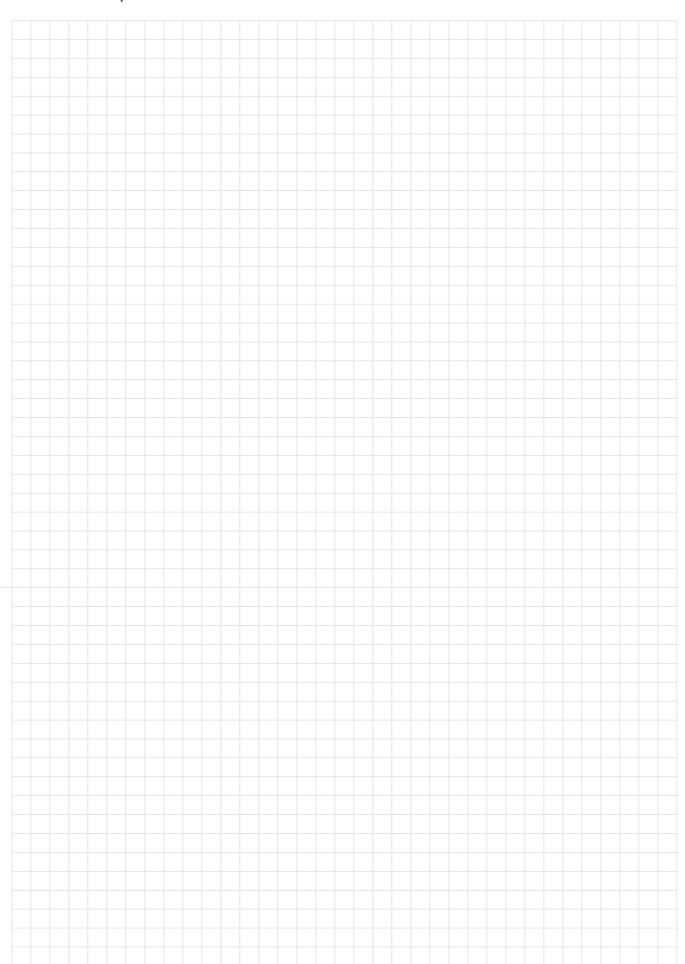
Lengths:

□ 305

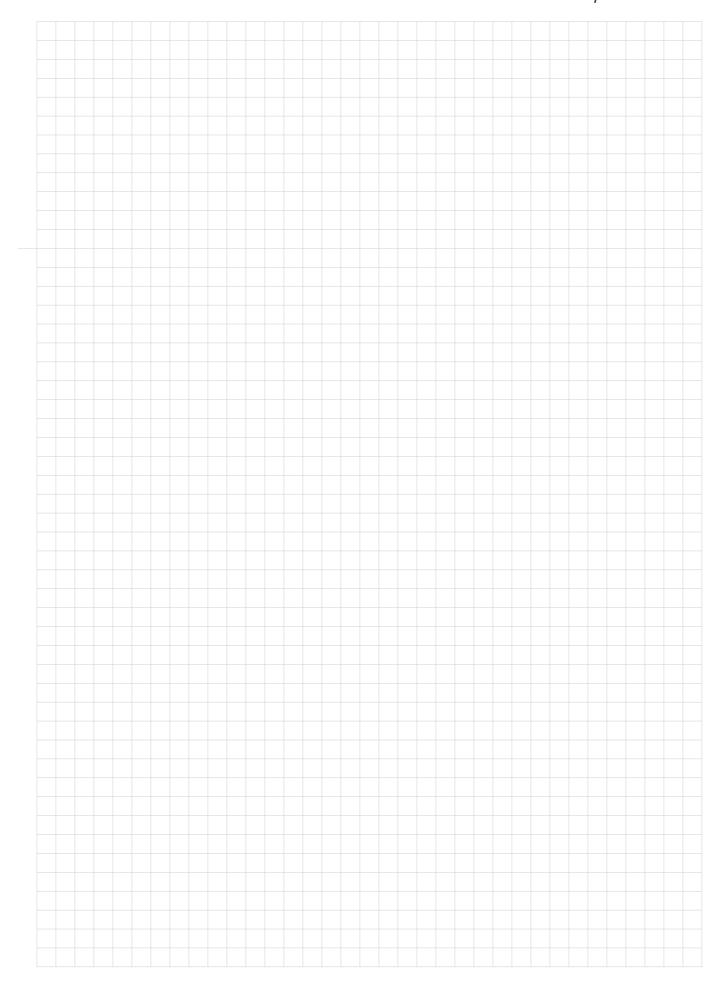
- 2,400 mm piece(s)
- 2,800 mm _ piece(s)

ACCESSORIES











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SYSTEM SOLUTIONS FOR SOPHISTICATED FRAMELESS GLASS ARCHITECTURE AS WELL AS THE SECURE ATTACHMENT OF ADD-ON PIECES TO ETICS

As a leading supplier, GLASSLINE develops, produces and distributes high-quality system solutions in the areas of point fixing systems, all-glass railing systems, frameless canopy constructions and systems with thermal separation for secure attachment of add-on elements to building envelopes.

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- All drawings are example applications. GLASSLINE assumes no warranty or liability for any transferable applications.
- Technical and constructional modifications are reserved.
 All screw connections are to be permanently secured against loosening, such as through gluing.
 The pressure-resistant insulating elements are to be protected against UV radiation and weather influences.
- Object-specific application as well as verifications of load application and transfer are to be checked or carried out on-site.

